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# Hydrogeology

of the Lost Lake Aquifer System In The Wilton-Washburn Area McLean County North Dakota

> By Allen E. Comeskey

North Dakota Ground-Water Studies Number 93 North Dakota State Water Commission Vernon Fahy, State Engineer



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HYDROGEOLOGY OF THE LOST LAKE AQUIFER

IN THE WILTON–WASHBURN AREA

#### MCLEAN COUNTY NORTH DAKOTA

# ND STATE WATER COMMUNCTION

North Dakota Ground–Water Studies Number 93

By

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# CONTENTS

	Page
Introduction	. 1
Statement of Purpose	1
Location	1
Previous Investigations	1
Location Numbering System	3
Present Water Supply	3
Acknowledgements	5
Methods	5
Hydrogeology	5
Water Levels	12
Water Quality	22
Production Well #3	23
Pump Test	23
Summary and Conclusions	24
References	25
Appendix	26
Test Hole Logs	27
Additional Water Levels	58
Table 3 Chemical Analysis	61
Table 4 Explanation of Chemical Analysis	62
Plates	Back cover

#### INTRODUCTION

#### STATEMENT OF PURPOSE

On October 10, 1985 the city of Wilton and the State Water Commission entered into agreement to conduct a study to locate a supplemental water supply. Wilton's present system is inadequate to neither meet peak demands nor to supply the city's treatment facility at its designed capacity.

The goals of the study were to better characterize the deposits of the Lost Lake aquifer in the vicinity of Wilton's well field and to ascertain the variability and distribution of the chemical quality of the water.

#### LOCATION

Wilton is located in the southeast corner of McLean County. Wilton's well field, which is completed in the Lost Lake aquifer, is located about 8 miles northwest of the city in Sections 2 and 3, Township 143 North, Range 81 West (fig. 1). Test drilling was conducted in Sections 2, 3, and 4, Township 143 North, Range 81 West; and Section 35, Township 144 North, Range 81 West.

#### PREVIOUS INVESTIGATIONS

Two recent investigations have dealt specifically with the Lost Lake aquifer. Klausing (1974) drilled 18 test holes in or around the aquifer from 1966 to 1970. On pages 38 through 39 of the McLean County Ground-Water Study, part III, he discusses the location, areal extent, nature of the sediments, water levels, and water quality. The configuration of the buried valley is represented on plate 1, the aquifer boundaries on plate 2, and geologic cross-sections on plate 3.

Naplin (1979) conducted additional drilling during the 1973 field season and better characterized a portion of the aquifer in which Wilton completed its production wells. On



FIGURE I.-Study Area Location.

pages 26 through 29 of North Dakota Ground-Water Studies No. 81 he describes the lithology, thickness, hydrologic properties, and water quality. Aquifer boundaries and the potentiometric surface are depicted in figure 5. Table 2 contains analysis of the chemical quality of the water. Geologic cross-sections of the Lost Lake aquifer are presented on plate 2.

#### LOCATION NUMBERING SYSTEMS

The system for denoting the location of a test hole or observation well is based on the federal system of rectangular surveys of public land. The first and second numbers indicate Township North and Range West of the 5th Principal Meridian and base line (fig. 2). The third number indicates the Section. The letters A, B, C, and D designate respectively the northeast, northwest, southwest, and southeast quarter Section (160 acre tract), quarter-quarter Section (40 acre tract) and quarter-quarter-quarter Section (10 acre tract). Therefore a well denoted by 143-081-04AAA would be located in NE1/4 NE1/4 NE1/4 of Section 04, Township 143 North, Range 81 West. Consecutive terminal numbers are added if more than one well is located in a 10 acre tract, for example,  $143-81-02BBB_1$  and  $143-81-02BBB_2$ .

#### PRESENT WATER SUPPLY

Wilton's present production wells are located at 143-81-02BCC and 143-81-03ADD. Well #1 (143-81-02BCC) is 55 feet deep, constructed of 8 inch-diameter casing and screened from 25 to 35 and from 50 to 55 feet. Well #2 (143-81-03ADD) is 85 feet deep, constructed of 12 inch-diameter casing and is screened from 65 to 85 feet. Wilton holds water permit #2173 which authorizes the withdrawal of 200 acre-feet per year at a rate of 400 gallons per minute. The water treatment plant is designed to operate at 200 gallons per minute. Wilton used an average of 77 acre-feet per year from 1975 to 1983. The wells are alternately pumped at one week intervals at about



FIGURE 2.-Location Numbering System.

120 and 140 gallons per minute respectively. Rodney Peterson of the city of Wilton says both production wells are experiencing substantial water level declines and require the one week intervals to recover. Neither well can sustain the 200 gallons per minute needed to operate the treatment plant at capacity. The 120 to 140 gallons per minute presently produced cannot meet Wilton's peak demands during the summer months.

#### ACKNOWLEDGEMENTS

Special thanks are due Rodney Peterson and Merton Hansen of the city of Wilton for their assistance and information and to Joseph Denault, Tod DeMontigny, Kent Rood, and William Sawiki for permission to conduct exploratory drilling on their properties.

#### **METHODS**

The study was accomplished by means of: 1) test drilling, which includes the recording of lithologic logs and borehole geophysical logs, and observation well construction; 2) water sample collection and analysis; and 3) water level monitoring.

Test drilling was conducted on August 8 and November 1 through 15, 1985 and May 2 through June 6, 1986. Twenty-six locations were drilled totaling 6,956 feet (a map showing the locations of all test holes is found on plate 1). Twenty-one observation wells were constructed. Water samples were collected on December 4 and 5, 1985 and June 6 through 9, 1986. Water levels were measured December 1985 through January 1986 and June 13 through July 10, 1986.

Test drilling was accomplished by the forward mud-rotary method generally using a 4 3/4 inch bit. Lithologic logs are written records of the materials encountered by the drill and are based on samples obtained from the drilling mud. These are compiled by the geologist. Geophysical logs are graphs of the electrical properties of the materials penetrated by the bore hole. The lithologic and geophysical logs have been included in the appendix. Observation wells provide access to the water contained in the aquifer by means

of 1 1/4 inch diameter pvc pipe and 1 1/4 inch pvc well screen of various slot sizes. Water samples were obtained by air lifting the water from the wells with air lines inserted into the wells and connected to portable compressors. These samples are sent to the State Water Commission Laboratory for analysis. Results of the analyses are found in table 3. The significance of these results are found in table 4 in the appendix. Water levels are obtained by inserting a steel tape into the well and measuring depth to water. Continuous water level recorders were also installed on selected wells. Water level data is included with the test hole logs in the appendix.

#### HYDROGEOLOGY

The Lost Lake aquifer system is associated with a buried valley. The valley is filled with fluvial silt, sand, and gravel; lacustrine clay and silt; glacial till; and ice contact deposits. Southwest of the study area it intersects the Painted Woods Creek aquifer which both Klausing (1974) and Naplin (1979) considered to be hydraulically connected to it. Northeast of the study area it extends into Sheridan County.

Naplin (1979) interpreted the sediments of the Lost Lake aquifer to be continuous but interrupted by a large lens of silt and clay to the northeast. Additional drilling revealed that locally it is several units composed of coarse sediments interbedded in silt and clay and having a limited hydraulic connection.

This study identified five distinct aquifer units within the study area as follows: 1) a surficial unit, 2) a shallow confined unit in which production well #1 is completed, 3) a shallow confined unit in which production well #2 is completed, 4) an intermediate confined unit, and 5) a deep confined unit.

The surficial unit ranges from 5 to 40 feet thick (fig. 3). It is composed of very coarse sand and gravel up to one inch in diameter. Grains are rounded and composed of carbonates and silicates. At higher elevations it is unsaturated and oxidized. Portions of this deposit are confined by clay or till.



FIGURE 3 - Thickness of surficial aquifer.

These sediments may be collapsed outwash, being deposited on stagnant ice and then draped over the land surface as glacial ice melted out from under them (plate 2, unit A). This would account for the variability in thickness and its location on hills and slopes. The sediment may be discontinuous, resulting in isolated patches of limited areal extent. These isolated patches may not contain enough water to support development of a water supply.

The shallow confined unit in which production well #1 is completed ranges from 19 to 80 feet thick (fig. 4). Depth to the aquifer ranges from 7 to 27 feet. It is about 1,600 feet long and 800 feet wide.

It is composed of fine sand to coarse gravel with predominantly fine and medium sand. Grains are rounded and composed of quartz. The aquifer is isolated, being enclosed in silt and clay (plate 2, cross-section D-D' and H-H', unit B). This may imply an origin as an ice contact deposit left as the glacial ice melted.

The shallow confined unit in which production well #2 is completed ranges from 52 to 57 feet in thickness and is interbedded with silt and clay (plate 2, cross-section H-H', unit C). Depth to the aquifer ranges from 48 to 63 feet. It is about 500 feet long and 500 feet wide (fig. 5). It is composed of fine sand to coarse gravel with predominantly medium to very coarse sand. Grains are rounded and composed of carbonates with some silicates. It, too, is an isolated deposit enclosed in silt and clay which may imply an ice contact origin.

The intermediate confined aquifer is from 50 to 149 feet thick (fig. 6). Depth to the aquifer ranges from 98 to 177 feet. Within the study area it is about 6,600 feet long and 1,000 to 3,700 feet wide. It is composed of fine to very coarse sand with predominantly very coarse sand. Grains are rounded and composed of quartz. The sediments lie directly on bedrock and are enclosed in silt and sandy clay (plate 2, unit D). The origin of the deposit may be either fluvial or an asker deposited in a lacustrine environment as suggested by its sinuous nature and the adjacent silt and clay.







FIGURE 6 - Thickness of intermediate confined aquifer.

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The deep confined aquifer occupies the deepest part of the buried valley where it is incised into bedrock and overlain by silt and clay (plate 2, unit E). It is not continuous along the long axis of the valley but has been truncated by low permeability sediments, effectively dividing it into two separate sections (fig. 7). Thickness ranges from 9 to 42 feet. The eastern portion is about 3,400 feet long and 400 feet wide. The western portion is about 2,300 feet long and 1,500 feet wide. It is composed of very coarse sand and coarse gravel with predominantly medium to coarse gravel. Grains are angular to rounded and composed predominantly of carbonates with some detrital lignite and silicates. The probable origin of the deposit is a preglacial fluvial sediment as suggested by the lack of shield silicates.

#### WATER LEVELS

One observation well is completed in the surficial aquifer. Observation well 11738 has a water level elevation of 1,685.41 feet. Depth to water is 7.18 feet and the aquifer has a saturated thickness of 29 feet.

Four observation wells are completed in the shallow confined aquifer in which production well #1 is completed. Observation well 3898 was completed in 1973 before the production well was constructed. On October 29, 1973 the water level elevation was 1,697.7 feet. On January 16, 1986 the water level elevation was 1,687.41 feet. This is a decline of about 10 feet.

Water level elevations range from 1,688.11 feet in the east to 1,687.17 feet near the production well on January 20, 1986. Gradients are toward the production well at about .3 feet per mile from the west to about 9.2 feet per mile from the east (fig. 8).

There is also an upward vertical gradient. Observation well 11731 is screened from 60 to 65 feet and has a water level elevation of 1,688.11 feet. Observation well 3898 is screened from 31 to 34 feet and has a water level elevation of 1,687.17 feet.

Production well #1 was pumped for 20 hours at 120 gallons per minute on January



FIGURE 7 - Boundary and thickness values of deep confined aquifer.



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20, 1986. On January 21, 1986 all observation wells were measured to determine which water levels had responded to the pumping. The water level in the production well was also measured to determine the amount of drawdown it is experiencing and how well it recovers. Water levels in observation wells 3898, 11722, 11615, 11731, and 8949 responded to the pumping.

Table 1 displays the declines of water levels observed at each well. On January 22, 1986 the water level in city well 1 had recovered 11.5 feet.

Well	Distance from Production Well (ft.)	Decline (ft)	
11615 11731 8949 11722 3898 City well 1	740 470 2000 540 140	$\begin{array}{c} 0.10 \\ 0.30 \\ 0.32 \\ 0.41 \\ 1.80 \\ 12.43 \end{array}$	

Table 1. – Water Level	Declines A	After 20	Hours	Pumping	of
	City Well	l 1			

One observation well is completed in the shallow confined unit in which production well #2 is completed. On November 14, 1973 the water level elevation was 1693.49 feet. On November 9, 1985 the water level elevation was 1654.41 feet. This is a decline of about 39 feet.

Production well #2 was also pumped for 20 hours at 140 gallons per minute on March 4, 1986. Water levels were measured on March 5, 1986. The water level in well 8950 was the only one affected though its response was obscured by barometric pressure changes and snow melt.

There are seven observation wells completed in the intermediate confined aquifer. Water level elevations on April 10, 1986 ranged from 1660.73 feet at 11729 to 1658.74 feet



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Local Rec: 7 [ No Processing | Label OFF | Export OFF | Edited ] NO HOLDINGS IN NDS - NO OTHER HOLDINGS Rec stat: n Entered: 19961219 Replaced: Type: a ELv1: I Audn: Ctrl: Srce: d Lang: eng ELVI: m Forma t Conf: 0 Biog: MRec: Ctry: ndu Cont: t GPub: s Fict: 0 Indx: 0 Desc: Ills: ab Fest: 0 DtSt: s Dates: 1988. 41 #C NDS 099 GB1197.6.N9 +a NOR, 93-1 049 100 1 Comeskey, Allen E. 6 245 10 Hydrogeology of the Lost Lake Aquifer in the Wilton-Washburn area. McLean County, North Dakota / +c by Allen E. Comeskey. Bismarck, N.D. (900 East Boulevard, Bismarck 58505) : +b North 260 State Water Commission, \*c 1988. iA, 62 p. : \*b ill.. maps ; \*c 28 cm. 9 440 0 North Dakota ground-water studies, \*v no. 93 1 map %1 chart folded leaves in \$ pocket. 504 Includes bibliographical references (p. 25). DOES NOT CIRCULATE. MATERIAL MUST BE USED AT THE NORTH DAKOTA STATE WATER COMMISSION TECHNICAL REFERENCE LIBRARY. REQUESTS FOR PHOTOCOPIES WILL BE ACCEPTED BY THE NORTH DAKOTA STATE LIBRARY. 650 Hydrogeology #z North Dakota #z McLean County 0 Groundwater +z North Dakota +z McLean County. 650 North Dakota State Water Conservation Commission.

at 8939. The gradient is towards the west at about 2.9 feet per mile (fig. 9).

At location 143-081-02BBCB observation wells 11732 and 11733 are screened from 225 to 230 feet and 158 to 163 feet, respectively. On January 22, 1986 the water level elevations were 1,660.63 feet and 1,660.55 feet respectively indicating a slight upward vertical gradient.

The United States Geological Survey has been monitoring the water level in observation well 8939 since 1978. Water level elevations have naturally fluctuated from about 1,660.5 feet to 1,663 feet (fig. 10). These fluctuations do not appear to be related to the amount of precipitation received in the area (fig. 11).

The Painted Woods Golf Club in Washburn has its irrigation well completed in this aquifer at 143–081–03BAAD. This well was constructed in 1983 and was used during the 1984 and 1985 seasons. In 1984 the golf course pumped 50.1 acre-feet and in 1985 it pumped 36.3 acre-feet at a rate of 300 gallons per minute. Effects of the pumping are reflected in the water levels in observation well 8939 (143–081–03BAA, fig. 10). Water levels declined about 3.5 feet during the 1984 pumping season and recovered to the pre-pumping level. Water levels declined about 5.5 feet during the 1985 pumping season. Recovery is not as complete as from the 1984 season resulting in a deficit of about 1.5 feet. It appears that the effects of the pumping are superimposed on a natural trend of declining water levels. Since there are about 122 feet of available drawdown, the maximum water level decline represents only 4.5% of what is available.

Continuous water level recorders were installed on observation wells 8939, 11770, 11739, 11732, and 11733 from June 13 through 20 and July 2 through 10, 1986. The extent and degree of the impact of the pumping of the golf course irrigation well was observed through the aquifer and surrounding sediments. Table 2 presents representative declines of water levels during pumping at various distances from the irrigation well.

143-81-03BAA



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PRECIPITATION AT WILTON

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FIGURE 11 - Precipitation at Wilton

Pumping Period	Well	distance from prod. well (ft.)	Drawdown (ft.)
June 16 through 18	8939 11770 11769	600 1500 800	3.2 2.1 2.8
July 5 through 9	8939 11733	600 2800	3.4 1.6

## Table 2. – Drawdown in Intermediate Confined Aquifer During Pumping of Painted Woods Golf Course Irrigation Well

Water level declines due to pumping of the irrigation well were less than anticipated, possibly indicating leakage from the surrounding sediments. Table 2 also compares the water level changes in well 11769 with changes in 8939. Well 11769 is completed in the silty and sandy clays that envelope the intermediate confined aquifer. A continuous record water level recorder was also installed on 11769 to detect effects from pumping of the irrigation well. Even though the coarse sediments that comprise the intermediate confined aquifer are of limited areal extent, water available for withdrawal will be supplemented by leakage from the surrounding sediments.

Water level elevations are noted beside the observation wells completed in the deep confined aquifer on figure 12. Water level elevations of the eastern portion range from 1708.85 to 1706.22 feet. The gradient is roughly to the west at about 11.4 feet per mile. Water level elevations of the western portion range from 1668.2 to 1658.1 feet. The gradient is roughly to the west or northwest at about 12.8 feet per mile. There is about a 38 foot difference between water level elevations of the two sections of aquifer.



FIGURE 12 - Water levels of deep confined aquifer.

#### WATER QUALITY

Water of the surficial aquifer as represented by a sample from well 11738 is sodium bicarbonate type. Total dissolved solids are 742 milligrams per liter (table 3). Hardness is 380 milligrams per liter. There are also isolated near surface sand units. Observation well 11725 is completed in one of these. A sample from this well contains 1,950 milligrams per liter total dissolved solids. The isolated nature is a major factor resulting in the more mineralized water. It is likely that other isolated deposits would contain water of similar quality.

Water of the shallow confined aquifer in which production well #1 is completed ranges from a calcium to sodium bicarbonate type. Total dissolved solids range from 367 to 1,220 milligrams per liter. Hardness ranges from 280 to 350 milligrams per liter.

Water quality is vertically stratified. Water derived directly from precipitation forms a layer above more mineralized water found at depth. Within 40 feet of the surface the water is a calcium bicarbonate type. Total dissolved solids are 381 milligrams per liter. At 60 feet the water is a sodium bicarbonate type. Total dissolved solids are 1,220 milligrams per liter. Production well #1 is screened from 25 to 35 feet and 50 to 55 feet. Water from the production well appears to be a blend of the two types of water and the concentration of total dissolved solids is 700 milligrams per liter.

Water from the shallow confined aquifer in which production well #2 is completed is a calcium bicarbonate type. Total dissolved solids range from 593 to 796 milligrams per liter. Hardness ranges from 310 to 340 milligrams per liter.

Water quality in the intermediate confined aquifer is a sodium bicarbonate type. Total dissolved solids range from 821 to 1,310 milligrams per liter. Hardness ranges from 67 to 370 milligrams per liter.

Water quality within the intermediate confined aquifer is variable both vertically and laterally. Observation wells 11732 and 11733 are screened from 225 to 230 feet and 158 to 163 feet respectively at location 143–081–02BBCB. Total dissolved solids were 1,310

and 1,210 milligrams per liter respectively. The greatest concentration of dissolved solids is encountered at 143-081-02BBCB from well 11732. The lowest concentration of dissolved solids was encountered at 143-081-03BAA at 821 milligrams per liter from well 8939.

Water from the deep confined aquifer is a sodium bicarbonate type. Total dissolved solids range from 781 to 1,300 milligrams per liter. Hardness ranges from 144 to 340 milligrams per liter. Water quality is generally better in the western portion of the aquifer.

#### **PRODUCTION WELL #3**

Based on the findings of this study, Production well #3 was located at 143-081-03ABB. It was drilled and constructed from October 2 to 19, 1987. After completion, a 24 hour pump test was conducted from October 20 to 21.

The well is 212 feet deep. It is constructed of 165 feet of 12.75 inch O.D. steel casing weighing 49.56 pounds per lineal foot. Fifty feet of 11 inch O.D. #24 slot, stainless steel wire wrap screen is welded to the bottom of the casing. The screened interval is from 162 to 212 feet below land surface. The screen was sand packed with sand and backfilled to 76 feet below land surface with unsorted gravel. Development consisted of airlifting and jetting. Following development, grout was emplaced from 50 to 76 feet, isolating the surficial aquifer from the intermediate confined aquifer. It was then backfilled to surface with gravel.

#### PUMP TEST

A 24 hour pump test was conducted for well #3 on October 20 and 21, 1987. The well was pumped at about 317 gallons per minute. Drawdown and recovery were recorded for the production well and continuous record water level recorders were installed on observation wells 11771 and 11733. After 24 hours 97.35 feet of drawdown were recorded. The specific capacity is 3.3 gallons per minute per foot of drawdown. The transmissivity is

calculated from the production well data at  $3,086 \text{ ft}^2/\text{day}$ .

#### SUMMARY AND CONCLUSIONS

The Lost Lake aquifer system occupies a buried valley that trends northeast from the Missouri River south of Washburn, through southeastern McLean County into Sheridan County. Sediments filling the buried valley are composed of fluvial silt, sand, and gravel; lacustrine clay and silt; glacial till; and ice contact deposits. Five aquifer units were identified within these sediments. They are as follows: 1) a surficial unit, 2) two shallow confined units, 3) an intermediate confined unit, and 4) a deep confined unit.

Wilton's present production wells are completed in the two shallow confined units. These will not support any further development due to their limited area extent. Remaining units have characteristics both favorable and unfavorable to development of a municipal supply. The surficial unit, though possessing superior quality water, may be too discontinuous to provide adequate quantity. The deep unit, though possessing adequate quantity, was lacking acceptable quality water. The intermediate confined unit has water with quality compatible with the needs of the city and has the areal extent and saturated thickness to support the development of a municipal supply.

Water quality within the intermediate confined unit varies both laterally and vertically, the lower dissolved solids occurring in the vicinity of 143–081–03BAA, and generally lower dissolved solids occurring near the top of the aquifer. The Painted Woods Golf Course irrigation well is located at 143–081–03BAAD and water levels will decline in its vicinity when being pumped. Siting a production well will be a compromise between utilizing the better quality water found in the vicinity of 143–081–03BAA and minimizing interference from pumping of the irrigation well. By screening only the upper portion of the aquifer, thus reducing the available drawdown to the top of the screen, the additional water level decline caused by pumping of the irrigation well will be more significant and should be considered.

# REFERENCES

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- Klausing, R.L., 1974, Ground-water resources of McLean County, North Dakota: County Ground-Water Studies 19, part 3.
- Naplin, Charles E., 1979, Geohydrology of the Washburn–Wilton area, Burleigh and McLean Counties, North Dakota: North Dakota Ground–Water Studies 81.

APPENDIX

### TEST HOLE LOGS

Grain size determination is based on the Wentworth (1922) size scale. Color description is based on the Geological Society of America (1963) rock color chart. Geophysical logs are single point resistance.



LOCATION: 143-81-02BACH ELEVATION: approx. 1710 (FT, MSL) DATE DRILLED: 11/4/85

DEPTH: 240 (FT)





LOCATION: 143-81-02BACC2

DATE DRILLED: 11/4/85 DEPTH: 43 (FT)

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ELEVATION: 1702.6 (FT, MSL)

POTENTIAL (MV)	RESISTANCE (OHMS)		DESCRIPTION OF DEPOSITS Glacial Drift
2		0 - 16 16 - 22	Clay, black to gray Silt, brown, clayey, slightly carbonaceous
	- 20	22 - 40	Sand and gravel, coarse sand to gravel 1" dia., predom. very coarse sand and fine gravel, subrounded to rounded
	- 40	40 - 43	Silt, yellow brown, slightly clayey
			Observation Well
			Depth: 40'
	- 60		
			Water Level
			12/4/85 8.45 1/16/86 8.58
			1/20/86 8/57 1/21/86 8 59
			1/22/86 8.58
			2/18/86 8.61 2/20/86 8.63
			3/4/86 8.41
	- 100		4/10/86 7.6
			4/22/86 7.36
5			
	- 120		
	120		
	8		
	- 140		
	- 160		
	- 180		
	- 200		
	220		
	~~~~		
	240		

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ELEVATION:	1731.9		DEPTH: 236 (FT)
(* 1, 1136)			<b>N</b> (1)
POTENTIAL	. ( <u>MV)</u>	RESISTANCE (OHMS)	DESCRIPTION OF DEPOSITS Glacial Drift
2	2	1	0 - 4 Sand, coarse, oxid.
			clayey, oxid. ) 8 -14 Sand, coarse sand to fine
		- 20	gravel, predom very coarse sand
			14 -20 Silt, yellowish drange, oxid. 20 -32 Sand, fine grading to coarse by
		- 40	32 -47 Gravel, Coarse Sand to gravel 21 "
		5	dia., rounded, oxid. 47-100 Clay, olive gray, silty, sandy,
			5
		- 80 5	
		5	
		5	
		- 100	100-124 Clay, olive gray (lacustrine)
		2	
		- 120	
			200' some interbedded clay
		- 140	>
			•
	1		>
	1		
		5	>
	8	- 180 2	>
		- F	Hell Creek Formation
		3	
			234-236 Claystone, brown, tight, waxy
			Depth: 230' 5.I.: 225'-230'
		- 220 2	Water Level
			2 12/4/85 71.78 1/16/86 71.10
			1/20/86 71.12 1/21/86 71.22
	L	240	2/18/86 71.12
			3/4/86 70.93 3/5/86 71.00
			4/10/86 71.39 7/2/86 73.22

LOCATION: 143-81-02BBCB1

DATE DRILLED: 11/6/85

LOCATION: 143-81-0288CB2

ELEVATION: 1732.4 (FT, MSL) DATE DRILLED: 11/6/85 DEPTH: 165 (FT)

POTENTIAL (MV)	RESISTANCE (OHMS)		DESCRIPTION OF DEPOSITS
		0 - 10	Glacial Drift Clay, dark yellowish orange,
		10 - 32	silty, oxid. Sand, fine to coarse
	- 20		x
		32 - 40	Gravel, coarse sand to l" dia. predom. א" dia., rounded, oxid.
	- 40	40 - 46	Sand, coarse, oxid. to 44'
		46 - 61	Clay, clive gray, silty, pebbly (till)
	- 60	61 - 66 66 -101	Gravel Clay, olive gray, silty, pebbly (till)
	- 80		
	- 100	101-125	Clay, olive gray, silty
	- 120	125-165	Sand, fine to coarse, predom. medium, rounded, interbedded clay to 153'
	- 140		
			<u>Observation Well</u> Depth: 163' S.I.: 158'- 163'
	- 160		<u>Water Level</u> 12/5/85 72.94 1/16/86 71.67 1/20/86 71.70
	- 180		1/20.86 71.82 1/22/86 71.85 2/18/86 71.68 2/20/86 71.79
	- 200		3/4/86 71.56 3/5/86 71.60 4/10/86 71.98 6/3/86 74.40 6/19/86 74.97 7/2/86 73.84
	- 220		7/2/86 73.81 7/3/86 73.63 7/10/86 74.65
	,		
	L 240		





LOCATION: 143-81-028CAC2

DATE DRILLED: 11/6/85

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#### DEPTH: 75

ELEVATION: 1702.3 (FT, MSL)			DEPTH: 75 (FT)
DOTENTIAL (MV)	RESISTANCE (OHMS)		DESCRIPTION OF DEPOSITS
POTENTIAL (MV)			Glacial Drift
	- 20	0 - 7 7 -20 20 -67	Clay, gray, mottled, oxid. Sand and gravel, very coarse sand to gravel, " dia., subangular to rounded Sand, fine to very coarse, predom. medium and coarse, subrounded
	- 40		
	- 60	67 -75	Silt, clayey
	- 80		<u>Observation Well</u> Depth: 65' S.I.: 60'- 65'
	- 100		Water Level 12/4/85 13.91 1/16/86 14.11
	- 120		1/20/86 14.19 1/21/86 14.49 1/22/86 14.60 2/18/86 14.93 2/20/86 14.67 3/4/86 14.10
	- 140		4/10/86 11.28 7/2/86 14.62
	- 160		
	- 180		
	- 200		r.
	- 220		
	240		



12/4/85	13.22
1/16/86	13.39
1/20/86	13.48
1/21/86	13.89
1/22/86	13.93
2/18/86	14.21
2/20/86	13,91
3/4/86	13.24
3/5/86	12.99
4/10/86	9.70
4/22/86	9.63
7/2/86	14.02



37

• Solaria



LOCATION: 143-81-02CBB ELEVATION: approx. 1745 (FT, MSL)

DEPTH: 80 (FT)

DATE DRILLED: 8/13/85

POTENTIAL (MV)	RESISTANCE (OHMS)	DESC	CRIPTION OF DEPOSITS
			Glacial Drift
		0 - 10 San f a s	d and gravel, fine sand to ine gravel, predom. coarse nd very coarse sand, ubrounded to rounded, oxid.
	- 20	10 - 22 San P 22 - 42 Sil	d, very fine to medium, predom. fine to medium, subangular to rounded it, slightly to moderately
	- 40	42 - 56 Cla P <sup>e</sup> gi	slayey, oxidized to 35 sy, olive gray, slightly sbbly, interbedded ravel (till)
	- 60	<u>H</u> 56 - 61 Si	ell Creek Formation Itstone, greenish gray, Clayey
		61 - 80 San	ndstone, greenish gray, fine grain, well sorted
	- 100		
	- 120		
	- 140		
	- 160		
	- 180		
	- 200		
	- 220		
	240		









LOCATION: 143-81-03ACCC

DATE DRILLED: 11/3/85

ELEVATION: approx. (FT, MSL)	1720		DEPTH: 80 (FT)
POTENTIAL (MV)	RESISTANCE (OHMS)	0(- 7 7 -12	DESCRIPTION OF DEPOSITS <u>Glacial Drift</u> Silt, black, carbonaceous Sand and gravel, predom. fine gravel, rounded, oxid.
	- 20	12 -23 23 -56	Clay, silty, oxid. to 16' Clay, olive gray, sandy, pebbly (till)
	- 40		
	- 60	56 -80	<u>Hell Creek Formation</u> Sandstone, fine grain, interbedded siltstone
	- 80		
	- 100		
	- 120		
	- 140		
	- 160		
	- 180		
	- 200		
	- 220		

- 240

- 160

- 180

- 200

- 220

- 240

DATE DRILLED: 8/13/85

# DEPTH: 100 (FT)

POTENTIAL (MV)

ELEVATION: 1704.7 (FT, MSL)

LOCATION: 143-81-03ADA1

RESISTANCE (OHMS)		DESCRIPTION OF DEPOSITS
		Glacial Drift
1	0 - 5	Sand, fine, oxid. Clav.d ark grav. carbonaceous
- 20	11 -18	Sand, fine to coarse; predom. medium, subangular to
	18 -31	subrounded Sand and gravel, coarse sand to gravel ¼" dia. subrounded to rounded
	31-100	Silt, dark gray, clayey,
- 40		interbedded, very fine sand
- 60		
- 80		
- 120		
1		
- 140		





LOCATION: 143-81-03ADBA

DATE DRILLED: 11/4/85

DEPTH: 260 (FT)





DATE DRILLED 11/14/85

LOCATION: 143-81-03ADBD2 ELEVATION: approx. 1700 (FT, MSL)

DEPTH 240 (FT)

.

POTENTIAL (MV)	RESISTANCE (OHMS)	Ļ	DESCRIPTION OF DEPOSITS Glacial Drift
	- 20	0 - 8 8 -11 11 -63	Gravel interbedded with silty clay Sand and gravel, very coarse sand to gravel ½" dia., rounded, oxid. Clay, olive gray, silty, very carbonaceous 20"- 48'
	- 40		
,	- 60	63 -92	Sand and gravel, coarse sand to gravel 4" dia., predom. very coarse sand to gravel 1/8" dia., rounded, carbonates
	- 80		and some silicates
		92-105	Clay, very sandy
	- 100	105-120	Sand, fine to coarse, predom. medium to coarse
	- 120	120-227	Clay, olive gray, silty, interbedded clayey silt and lignite
	- 140		
	- 160		
	- 180		
	- 200	227-236	Gravel to ኣ" dia., rounded, predom. carbonates
	- 220	236-240	<u>Hell Creek Formation</u> Claystone, brownish gray
	240		

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DATE DRILLED: 11/15/85

#### DEPTH: 80 (FT)

LOCATION: 143-81-03ADCD ELEVATION: approx. 1740 (FT, MSL)

POTENTIAL (MV)	RESISTANCE (OHMS)		DESCRIPTION OF DEPOSITS
		0 - 9	Glacial Drift Sand and gravel, coarse sand to gravel 1" dia., predom. rounded gravel to %" dia. oxid.
	- 20	9 -32 32 -40	Sand, coarse, well sorted, rounded Sand and gravel, as above
	- 40	40 -55	Clay, olive gray, silty, sandy, soft, oxid. 40'- 41' (till)
	- 60	55 -70 70 <b>~80</b>	Hell Creek Formation Claystone, interbedded siltstone Sandstone, greenish gray, fine grain
	- 80		
	- 100		
	- 120		
	- 140		
	- 160		
	- 180		
	200		
	- 220		

49



LOCATION: 143-81-03BABD

ELEVATION: (FT, MSL)

TEST HOLE 11769

		TEST HOLE	11768	
	LOCATION: 143-81-033BAD			DATE DRILLED: 5/28/86
	ELEVATION			DEPTH: 300
	(r), Mac)			(* 1)
	POTENTIAL (MV)	RESISTANCE (OHMS)		DESCRIPTION OF DEPOSITS
			0 - 16	Glacial Drift Gravel, very coarse sand to
				pebbles, angular to rounded,
			16 - 83	Silt, very clayey, soft,
		- 20		plastic, cohesive, interbedded, gravel, sandy clay, and
				clay, oxidized to 47 feet
		- 40		
		- 60		
•		60		
5		- 80	83 - 96	Clay, silty, sandy, pebbly, soft,
				(till)
	1		96 -100	Gravel very coarse sand to
		- 100	96 -100	pebbles, angular to round
_			100 -117	soft, plastic
		- 120	117-140	Clay, very sandy, soft, crumbly, interbedded silty clav
		.20		
•				
			140.160	
		- 140	140-160	soft, interbedded detrital
				lignite
•				
	•	- 160	160-201	Sand, clayey, very fine,
				Interbedded datritur righteo
		- 180		
		200	201-215	Clay, carbonaceous, interbedded
				sandy clay
•			215-262	Clay, sandy, carbonaceous
84		- 220		it.
		50 1		
		240		
		- 260	262-292	Gravel, coarse pebbles, round
				lacustrine and quartzite, interbedded clay
<b>a</b>				
ж 2		- 280		
•		1		Hell Creek Formation
			292-300	Sandstone, very fine, clayey
		- 300		
	1			Observation Well Denth: 268'
•				S.I.: 263'- 268'
		- 320		Water Level
				7/14/86 approx. 63.87'
		- 340		
•				
	the second s	- 360		





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LOCATION: 143-81-03CBBB

ELEVATION (FT, MSL)

DATE DRILLED: 5/21/86 DEPTH: 260 (FT)

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LOCATION: 143-81-04AAAD ELEVATION: (FT, MSL) DATE DRILLED: 5/21/86

0EPTH: 280 (FT)







LOCATION: 143-81-04ADAA

DEPTH: 300 (FT)



LUCATION IT OF COMMENT
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DATE DRILLED: 11/12/85 DEPTH: 140 (FT)

ELEVATION: approx. 1720 (FT, MSL)

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180

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POTENTIAL (MV)	RESISTANCE (OHMS)		DESCRIPTION OF DEPOSITS Glacial Drift
	- 20	0 -12 12 -26 26 -51	Gravel, very coarse sand to gravel 2" diapredom. 4 - 4" dia., rounded, oxid. Clay, yellow brown, silty, pebbly, oxid. to 18' Clay, olive gray, silty, interbedded with till
	- 40	51 -76	Clav. miltv, mandy, pebbly (till)
	- 60		
	- 80	76 -89	Clay (lacustrine)
		89 -99	Clay (till) as above
	- 100	99-113 113-116	Silt, clayey Clav, silty
	- 120	116-140	Hell Creek Formation Claystone, interbedded with sendstone
	- 140		
	- 160		
	- 180		
	- 200		
	- 220		
	240		

143-081-02BBB2

<u>Lost Lake</u>	aquifer		LS Elev	(msl,ft)=	1710.20 SI	(ft)= 37-40
Date	Depth to Water (ft)	WL Elev (msl,ft)		Date	Depth to Water (ft)	WL Elev (msl,ft)
11/14/73	35.96	1674.24		02/18/	86 34.29 86 34.37	1675.91 1675.83
01/16/86	34.15	1676.05		03/04/	86 33.90	1676.30
01/20/86	34.10	1676.10		03/05/	86 34.29	1675.91
01/21/86	34.42	1675.78		04/10/	86 34.16	1676.04
01/22/86	34.37	1675.83		07/02/	86 34.26	1675.94

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143-081-02BCCB

143-081-0 Lost Lake	e aquifer	Wilton # 1	<u>SI (ft)=</u> BB-35
Date	Depth to Water (ft)		к
01/17/86	22.39		
01/20/86	22.76		
01/21/86	35.19		
01/22/86	23.69	e 7	

143-081-02 Lost Lake	BCC1 aquifer		LS Elev (msl,ft)= 1705	5.40 <u>SI (f</u> t	)= 252-258
Date	Depth to Water (ft)	WL Elev (msl,ft)	Date	Depth to Water (ft)	WL Elev (msl,ft)
05/21/79	+1.26	1706.66		7	
06/28/79	+1.94	1707.34	05/18/82	+1.43	1706.83
07/31/79	+1.78	1707.18	06/29/82	+1.79	1707.19
08/24/79	+1.49	1706.89	07/27/82	+2.00	1707.40
09/25/79	+1.18	1706.58	08/25/82	+1.93	1707.33
10/25/79	+1.09	1706.49	09/30/82	+1.76	1707.16
03/20/80	+1.37	1706.77	05/04/83	+1.76	1707.16
04/23/80	+0.86	1706.26	05/31/83	+2.12	1707.52
05/21/80	+0.83	1706.23	08/29/83	+1.54	1706.94
06/23/80	+0.95	1706.35	09/29/83	+1.17	1706.57
07/21/80	+1.01	1706.41	10/27/83	+1.28	1706.68
08/21/80	+0.88	1706.28			
09/22/80	+1.04	1706.44	04/18/84	+1.30	1706.70
			05/16/84	+1.62	1707.02
04/30/81	+1.21	1706.61	06/27/84	+1.70	1707.10
06/02/81	+1.07	1706.47	07/26/84	+1.34	1706.74
06/24/81	+0.98	1706.38	09/20/84	+0.92	1706.32
08/24/81	+0.86	1706.26			
09/28/81	+0.82	1706.22	04/10/86	+0.74	1706.14
11/04/81	+0.77	1706.17	07/02/86	+0.83	1706.23
12/02/81	+0.66	1706.06			

#### 143-081-02BCC2 Lost Lake aquifer

LS Elev (msl,ft)= 1705.00 SI (ft)= 31-34

	Depth to	ML Elev	<b>D</b> = 4 -	Depth to	WL Elev
Date	Mater (Tt)	(MS1,TT)	Date	Mater (TT)	(MSI)TT)
10/29/73	7.30	1697.70	01/21/86	19.64	1685.36
			01/22/86	18.69	1686.31
08/20/85	17.30	1687.70	02/18/86	19.10	1685.90
08/21/85	18.60	1686.40	02/20/86	18.36	1686.64
10/09/85	17.64	1687.36	03/04/86	16.63	1688.37
			03/05/86	17.34	1687.66
01/16/86	17.59	1687.41	04/10/86	13.60	1691.40
01/20/86	17.83	1687.17	07/02/86	18.58	1686.42

143-081-03ADB Lost Lake aguifer

10 Elms (mal fd)	- 1701 40	CT 14	+)- 77-87
LS CLEV (MSI)TU	- 1/01.40	21 (1	(1 - 11 - 03)

Date	Depth to Hater (ft)	WL Elev (msl,ft)	Date	Depth to Water (ft)	WL Elev (msl,ft)
11/14/73	7.91	1693.49	01/22/86	45.80	1655.60
		Ganade and and effect from the store	02/18/86	44.32	1657.08
08/21/85	57.87	1643.53	02/20/86	45.05	1656.35
10/09/85	46.99	1654.41	03/04/86	45.40	1656.00
			03/05/86	46.18	1655.22
01/16/86	46.64	1654.76	04/10/86	42.08	1659.32
01/20/86	46.48	1654.92	07/02/86	38.54	1662.86
01/21/86	46.03	1655.37			

h	Depth to later (ft)	WL Elev (msl,ft)	Date	Depth to Water (ft)	
73	36.25	1659.05			
			05/18/82	35.12	
30/78	34.37	1660.93	06/29/82	32.64	
/26/78	34.35	1660.95	0//2//82	32.67	
/24/78	34.49	1660.81	08/25/82	33.07	
/06/78 -	34.60	1660.70	- 09/30/82	33.40	
/28/78	34.62	1660.68	11/03/82	33.07	
/26/78	34.49	1660.81	12/01/82	32.55	
/24/78	34.69	1660.61			
/25/78	34.72	1660.58	03/30/83	32.32	
/31/78	34.84	1660.46	05/04/83	32.45	
/30/78	34.60	1660.70	05/31/83	32.69	
			08/29/83	33.15	
5/22/79	33.09	1662.21	09/29/83	33.87	
6/27/79	33.34	1661.96	10/27/83	33.70	
7/31/79	33.62	1661.68	12/07/83	33.70	
3/24/79	33.94	1661.36			
9/25/79	34.46	1660.84	04/18/84	33.33	
0/25/79	34.71	1660.59	05/16/84	33.51	
1/20/79	35.00	1660.30	06/27/84	35.90	
			07/26/84	36.80	
2/20/80	33.83	1661.47	09/20/84	37.64	
3/20/80	33.94	1661.36	12/04/84	34.02	
/23/80	34.30	1661.00			
5/21/80	34.45	1660.85	01/16/86	34.86	
6/23/80	34.14	1661.16	01/20/86	34.87	
7/21/80	34.14	1661.16	01/21/86	35.00	
8/26/80	33.98	1661.32	01/22/86	35.03	
9/22/80	33.86	1661.44	02/18/86	34.87	
1/25/80	33.50	1661.80	02/20/86	34.94	
L/ L5/ 00	33.30		02/25/86	34.72	
4/30/81	33.65	1661.65	03/04/86	34.74	
6/02/81	33.86	1661.44	03/05/86	34.81	
5/24/81	33.83	1661.47	04/10/86	36.56	
8/05/81	33.69	1661.61	06/05/86	37.44	
8/26/81	33.85	1661.45	06/13/86	39.23	
0/28/81	33.05	1661.33	07/02/86	36.92	
1/04/81	36.02	1661 28	07/10/86	37.78	
2/02/01	74.02	1661.20	017 107 00		

#### <u>Lost Lake aquifer</u>

#### LS Elev (msl,ft)= 1695.30 SI (ft)= 157-163

54		
	2	

	S A R Specific pH Conductance			2.9 1060 8.12		7.4 1800 7.92	.6 690 8.06	16 2080 8.3	3.1 8,14	1.0 730 8.1	.5 624 7.7	1.5		19 2150 8 3	13 1280 8.24	14 2000 8.23	17 1750 8.34	24 8.7	5.9 8.19	10 2050 8,27	17 2000 8.3	4.3 1000 7.9	5.1 7.82		7.3 8.26	4.0 1425 8.07	11 1460 8.4	6.5 1120 8.0		14 2250 8.07	16 2080 8.3	4 623 8.18	:1.3 15 8.41	6.8 1520 8.29		2.5 2450 7.73	
	ess Percent arbonate			0 42		0 66	0 15	7 13	0 46	0 21	0 13	0 28		0 89	0 82	0 83	0 87	0 93	0 60	0 75	0 87	0 54	0 56		0 66	0 50	0 82	0 70		0 83	0 87	0 51	0 B3	0 65		38 34	
	Total Hardn CaCO <sub>3</sub> Nonce			380		350	280	285	330	320	310	340		110	180	180	140	67	370	260	130	300	390		340	380	140	180		190	144	340	170	300		1610 10	
	B) Total Dissolved Solids as			.17 742		.49 1220	.14 370	367	.25 700	.1 485	.43 796	£65 60°		1.7 1310	.63 1210	.8 1270	1.6 1290	2.3 1240	.5 1020	.66 1240	1.5 1290	. 26 821	.48 974	-	.51 1130	.5 825	.56 911	.43 697		1.4 1300	1250	.43 781	1.0 1100	.65 976		.3 1950	
( P	(F) (NO <sub>3</sub> ) (	-		.2 1.0		.4 1.0	0.1 1.	•	.18 1.0	.2 1.0	.3 2.0	.1 1.0		1.2 1.0 1	1.0 1.0	.6 1.0	.8 1.0	.6 1.0 5	.3 1.0	.5 1.0		.3 1.0	.4 1.0		.5 1.0	.4 1.0	1.1 1.9	6. 8.		.6 1.0 1	8.	.4 .3	.7 .5 1	.5 .2		.3 1.0	
CHEMICAL ANALYSES utiligrams per lifer except where indicated	(c1)			4 22		0 53	0 3.4	0.2	0 19	4 4.5	8 5.1	4 13		1 150	1.6 220	0 94	6 120	0 41	0 34	0 67	4 110	0 23	0 46		0 60	0 31	80	8 33	-	08		9 41	1 170	0 57		0 S7	
	3) (CO3) (SC			0		0 20	0	45	0 16	0	2	0		0 0	0	0 13	6 8	36 21	0 21	0 17	6 0	0 15	0 16		0 15	0 14	12 5	0	_	0 16	8 0	0 11	14 2	4 14		0 86(	_
	(K) (HCO		_	8.4 655		11 96]	5.4 34	4.3	7.1 53	11 464	5.4 38(	9.1 479		6.7 1110	7.5 928	7.0 1030	7.2 1090	3.8 93	1.0 817	9.6 960	6.8 1090	9.3 603	7.6 809		7.2 920	7.0 69	5.5 748	6.7 616		7.1 1050	4.5 1180	6.7 676	6.1 922	518 0.7		8.9 695	2
BLE 3 -	(Na) (QN			32 130		24 320	24 23	19 19	28 130	32 41	21 22	30 63		10 460	18 400	16 420	12 450	7 450	36 260	22 370	11 450	32 170	39 230		30 310	35 180	13 300	15 200		20 430	8.9 443	32 170	14 400	29 270	-	81 230	<u></u>
TA Analytical R	An) (Ca) (I			47 100		17 100	46 72	82	34 86	76 76	62 89	60 88		08 29	1 44	11 45	06 37	03 15	51 89 7	25 66	18 35	4 69	46 91		43 88	34 94	16 34	14 47	-	09 41	43	33 84	1 43	18 73	-	1 256	
y	iO <sub>2</sub> ) (Fe) (A	-		24 .05 .		28 .16 .	26 .93 .	29 1.8	24 .18 .	25 .07 .	24 2.9 .	28 2.2 .		21 .64 .	24 .06 .	25 .15 .	24 .29 .	. 06	24 .06 .	24 .05 .	25 .18 .	27 .03 .	26 4.6 .		26 1.6 .	25 .17 .	22 2.2 .	23 2.0 .	_	26 .46 .	33 .12	29 2.3 .	27 .29 .	26 1.4 .		26 4.7 1.	
	Date of (5 Collection			12/4/85		12/4/85	12/4/85	11/6/69	1/21/86	12/4/85	11/2/73	2/20/86		12/5/85	12/5/85	12/4/85	12/5/85	6/9/86	6/9/86	12/4/85	12/4/85	2/25/86	6/6/86		6/9/86	6/6/86	10/25/73	10/26/73		12/4/85	11/6/69	6/6/86	6/6/86	6/6/86		12/4/85	
	h Temp(°F)													30	63	03	03	68	63	83	83	63	06		63	68	63	73		73	58	68	63	63		0	-
	n Dept of Well (feet)			31-36		2AC2 60-65	CBC2 18-23	31-34	3CB 25-55	3A1 26-31	3B 80-83	38D 65-85	35	9CB1 225-2	BCB2 158-1	CAB 198-2	CBC <sub>1</sub> 198-2	8AA1 263-2	3AA2 158-1	JAD2 178-1	JBA 178-1	NA 157-1	AD 160-1		BDA 158-1	ABD 163-1	001 260-2	DD2 170-1		DBC 268-2	cc1 255-2	BAD 263-2	BDD 258-2	AAD 258-2		ACC2 35-4	
	Location			143-81-03AC		143-81-02BC	143-81-02BC	143-81-02BC	143-81-02BC	143-81-03AD	143-81-03AD	143-81-03AD		143-81-02BB	143-81-02BB	143-81-02BC	143-81-02BC	143-81-03AB	143-81-03AB	143-81-03AD	143-81-03AD	143-81-03BA	f 143-81-03BA	8	143-81-03AB	143-81-03BA	143-81-04AD	143-81-04AD		143-81-0280	143-81-02BC	143-81-03BE	143-81-03BB	143-81-0448		143-81-02BA	
	AQUIFERS Owner or Designation		Surficial aquifer	SWC #11738	Shallow Confined	SWC #11731	11722	3898	Wilton #1	SWC #11615	8950	Wilton #2	Intermediate	SWC #11732	SWC #11733	SWC #11727	SWC #11721	SWC #11770	SWC #11771	SWC #11735	SWC #11739	SWC #8939	Painted Woods Gol	Alluvial Sediment	SWC #11772	SWC #11769	SWC #8932	SWC #8932A	Deep Confined	SWC #11726	SWC #3897	SWC #11768	SWC #11767	SWC #11763	Misc.	SWC #11725	

TABLE 4 - Dissolved chemical constituents in water -- their effects upon usability and recommended concentration limits for domestic and municipal water supplies in North Dakota.

Constituent . or Parameter	Effects of dissolved constituents on water use	Suggested limits for drinking water in North Dakota	U.S. Public Health Service recommended limits for drinking water <sup>2</sup>	Constituent or Parameter	Effects of dissolved constituents on water use	Suggested limits for drinking water in North Dakota	U.S. Public Health Service recommended limits for drinking water <sup>2</sup>
Silica (Sio <sub>2</sub> )	No physiological significance			Chloride (cl)	Over 250 mg/1 may impart a salty taste, greatly excessive concentrations		250 mg/i
lron (Fe)	Concentrations over 0.1 mg/l will cause stain- ing of fixtures. Over 0.5 mg/l may impart		0.3 mg/l		may be physiologically harmful. Humans and animals may adapt to higher concentrations.		
	food and drink.			Flouride	Flouride helps prevent	Limits of 0.9 mg/l	Recommended limits depend on average of daily temperatures.
Manganese (Mn)	Produces black staining when present in amounts exceeding 0.05 mg/l		0.05 mg/l	(r)	ified limits. Higher concentrations cause mottled teeth.	LO 1.5 mg/1	Limits range from 0.6 mg/l at 32°C. to 1.7 mg/l at 10°C.
Cəlcium(Ca) ənd Məgnesium (Mg)	Calcium and magnesium are the primary causes of hardness. High concentra- tions may have a laxative effect on persons not accustomed to this type of water.			Nîtrate (NO <sub>3</sub> )	Over 45 mg/l can be toxic to infants. Larger Concentrations can be tolerated by adults. More than 200 mg/l may have a deleter- ious effect on livestock health	,	45 mg/l
Sodium (Na)	No physiological sig- nificance except for people on salt-free diets. Does have an effect on the irrigation usage of water.	•		Boron (B)	No physiological signl- ficance. Greater than 2.0 mg/l may be detri- mental to many plants		
Potassium (K)	Small amounts of potassium are essential to plant and animal nutrition.			Total dissolved solids	Persons may become accustomed to water containing 2,000 mg/l or more dissolved	0-500 mg/l - low 500-1400 mg/l averag 1400-2500 mg/l high over 2500 mg/l very	500 mg/l je
Bicarbonate	No definite significance,				solids.	hìgh	
and Carbonate (C03)	content will impart a flat taste to water.			Hardness (as CaCo3)	Increases soap consump- tion, but can be removed by a water-softening system.	0-200 mg/l - low 200-300 mg/l average 300-450 mg/l high over 450 mg/l very	
Sulfate	Combines with Calcium to	0-300 mg/l - low	250 mg/l			high	
(304)	500 mg/l tastes bitter and may be a laxative	over-700 mg/l - very high		рH	Should be between 6.0 and 9.0 for domestic consumption		
Percent Sodium and Sodium Ad- sorption Ratio (SAR)	Indicate the sodium hazard of irrigation water.			Specific Conductance	An electrical indication of total dissolved solids measured in micromhos per Centimeter at 25 <sup>0</sup> C. Used primarily for irrigation analyses.		

1. Schmid, R. W., 1965, Water Quality Explanation: North Dakota State Water Commission, unpublished report, File No. 989. 2. U.S. Public Health Service, 1962, Public Health Service Drinking Water Standards:

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62

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