

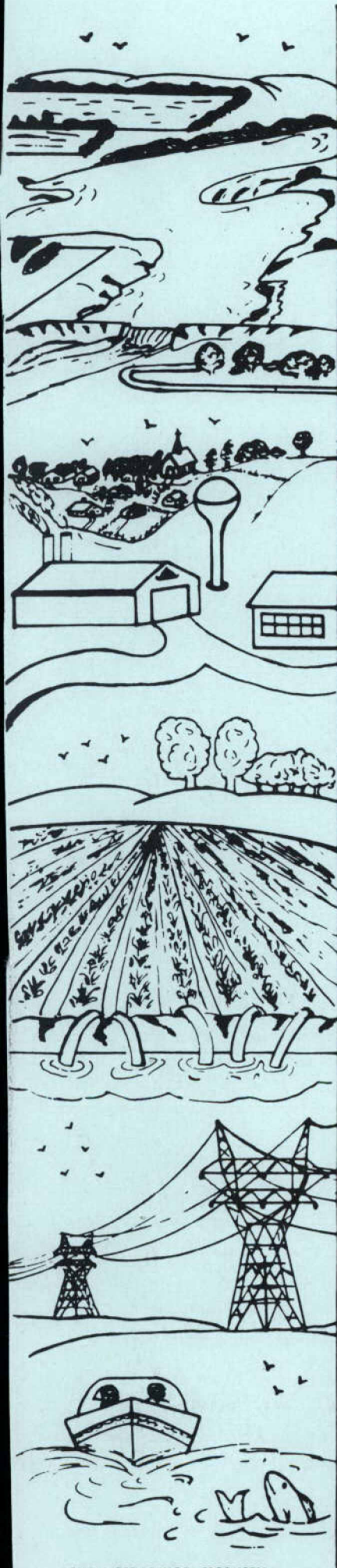
GROUND-WATER RESOURCES OF THE POWERS LAKE AREA
BURKE COUNTY, NORTH DAKOTA

NORTH DAKOTA GROUND-WATER STUDIES
NUMBER 85

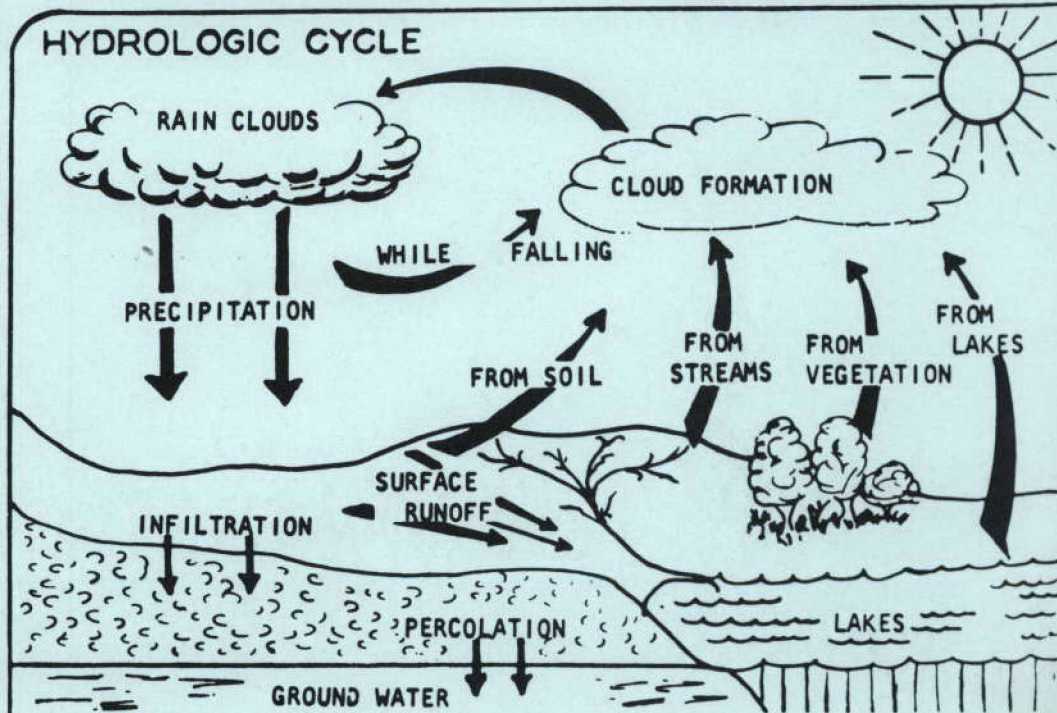
By
Allen Comeskey, Hydrologist
North Dakota State Water Commission

Published By
North Dakota State Water Commission
State Office Building
900 East Boulevard
Bismarck, North Dakota 58505

-1983-



HYDROLOGIC CYCLE



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INTRODUCTION

On September 1, 1977 the mayor of Powers Lake requested a study to be conducted by the North Dakota State Water Commission to locate a supplementary municipal water supply. The Water Commission approved sharing equally the estimated costs of \$7,260.00 with the city of Powers Lake. On July 7, 1978 the city of Powers Lake and the North Dakota State Water Commission entered into agreement to study the availability and quality of ground water in the vicinity of the city.

The study was conducted from June 6 to June 20, 1978 by the Water Commission drilling crew, equipment, and hydrologist. Nineteen test holes were drilled totaling 2,160 feet.

Location

The city of Powers Lake is located in the southwest corner of Burke County, North Dakota (fig. 1). Southern Burke County is located in the glaciated Missouri Plateau physiographic province (Simpson, 1929). The test drilling was conducted in Township 159 North, Range 92 West, Section 31 and Township 159 North, Range 93 West, Sections 25-28 and 34-36.

Present Water Supply

Powers Lake previously obtained its water from two wells located in town. Well #1 is located at 159-93-26JDD and is reported to be 103 feet deep. City well #2 is located at 159-93-35AAA and is reported to be 101 feet deep with the depth to the aquifer being 85 feet. The city if allowed to appropriate 220 acre-feet per year at a maximum rate of withdrawal of 110 gallons per minute.

After completion of this study, Powers Lake installed two wells in December, 1978. City well #3 is located at 159-93-36BAC. It penetrated

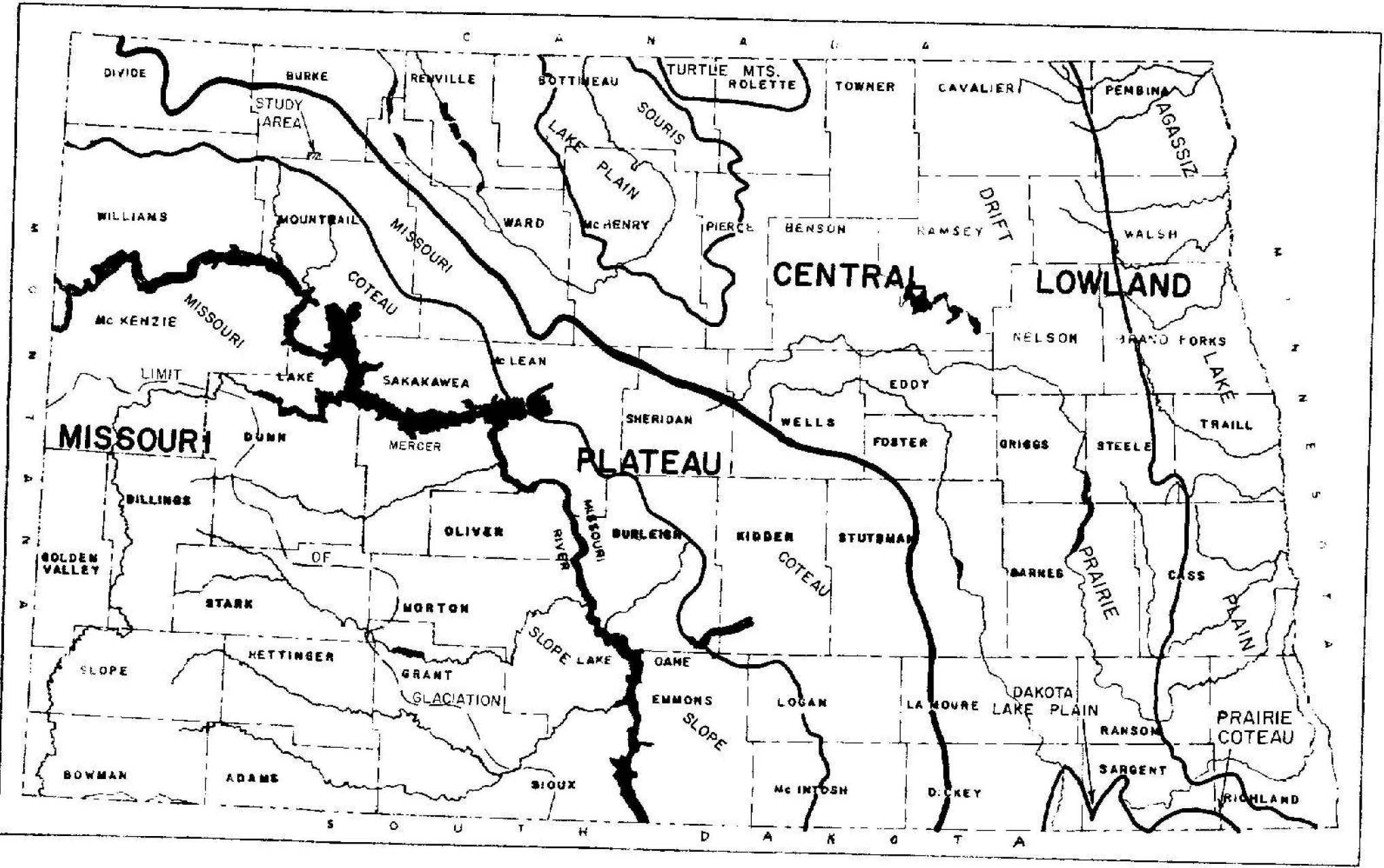


FIG. 1-STUDY AREA LOCATION

12 feet of sand and gravel from 65-71 feet and is screened from 66-77 feet. City well #4 is located at 159-93-36ABC. It penetrated 11 feet of sand and gravel from 62-73 feet and is screened from 64-73 feet.

Previous Investigations

In the USGS Water Supply Paper No. 598, pages 90-94, Simpson (1929) describes the general availability and quality of ground water from bedrock and glacial aquifers in Burke County. On page 91 he describes the numerous springs issuing from the morainal hills in the vicinity of Powers Lake. He also describes the general availability of water from the Fort Union Formation throughout the county.

In North Dakota Ground Water Study No. 23, pages 11-12 and 19, Paulson (1954) describes the origin and occurrence of water in the White Lake depression south of Powers Lake.

In North Dakota Ground Water Study No. 28, pages 53-57, Brookhart and Powell (1961) describes the results of their test drilling within the city limits of Powers Lake. They mention the occurrence of glacial and bedrock aquifers and the quantity and quality of water obtained from both.

In the North Dakota State Water Commission County Ground Water Study No. 14, pages 30 and 53-59, Armstrong (1971) describes the areal extent of and water quality in the Shell Creek aquifer which is in the vicinity of Powers Lake.

Location Numbering System

The system for denoting the location of a test hole or observation well is based on the federal system of rectangular surveys of public lands. The first and second numbers indicate township north and range west of the 5th

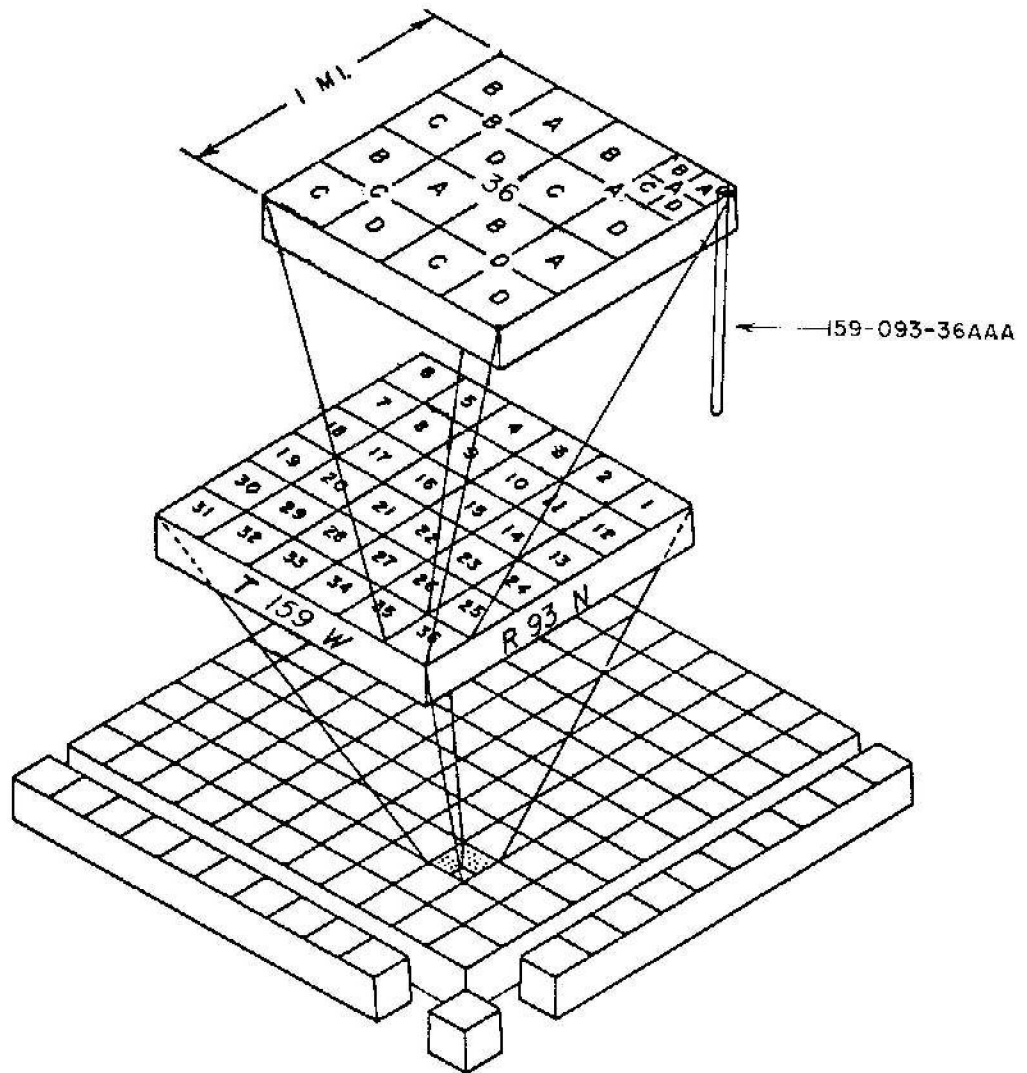


FIG. 2 WELL NUMBERING SYSTEM

Principal Meridian and base line. The third number refers to the section. The fourth, fifth, and sixth letters refer to quarter sections, quarter-quarter sections, and quarter-quarter-quarter sections lettered consecutively A through D in a counter-clockwise direction (fig. 2).

Bedrock Aquifers

Armstrong (1971) discussed bedrock formations which possess a potential as aquifers in Burke and Mountrail Counties. Pre-Cretaceous Formations were discussed as a unit. Depth to the top of the pre-Cretaceous Formations is projected to a depth greater than 3900 feet. Water quality is variable but expected to be too saline for most purposes.

The top of the Dakota Group is projected to be at a depth of 3,500 feet in Burke County. Yields to wells completed in this formation in Mountrail County yield an average of 290 gallons per minute with specific capacities between 0.4-3.0 gpm per foot of drawdown. The water is a sodium chloride type.

The Fox Hills-Hell Creek undifferentiated of Cretaceous age is projected at a depth of 1,100 to 1,300 feet and contains about 100 feet of sandstone with interbedded silt and clay. It is expected to yield a few gallons per minute, possibly under artesian conditions, of a soft, sodium bicarbonate type water.

The Fort Union Formation of Paleocene age is found directly beneath the glacial till. It is comprised of the Ludlow, Cannonball, and Tongue River members and is composed of interbedded sandstone, lignite, and shale. Yields are expected to be a few gallons per minute of a predominantly sodium bicarbonate type water.

GLACIAL AQUIFERS

White Lake Branch of the Shell Creek Aquifer

State Water Commission test holes No. 784, 785, 10092, 10093, 10094, 10095, 10096, 10097, 10100, 10104, 10105, and city wells 2, 3, and 4 appear to penetrate the edge of the White Lake Branch of the Shell Creek aquifer (fig. 3, table 1). Of these only 10092, 10096, 10100, and 10104 are completed as observation wells (table 1). The thickness ranges from 12 to 90 feet. Depth to the aquifer ranges from 50 to 100 feet. The elevation of the deposit lies between 2000 and 2150 feet above msl as seen in the cross sections (fig. 4 and plate 1). The aquifer is composed of predominantly medium to coarse sand and fine to medium gravel. Grains are generally subangular to subrounded, predominantly subangular, and composed of equal proportions of carbonates, silicates, and detrital shale with minor amounts of igneous, metamorphics, and detrital coal. There are minor amounts of interbedded silt and clay also. The general areal extent is shown in figure 5. The boundary conforms roughly to the walls of the White Lake depression and is more clearly defined where test holes can lend control.

The water level is highest in test hole No. 10104 at an elevation of 2197.45 feet above msl and decreases in wells 10100 and 10092 at 2193.86 and 2188.74 feet above msl respectively. The slope of the piezometric surface is steeper at first, declining 3.59 feet in 0.1 mile between 10104 and 10100. It becomes flatter between 10100 and 10092, declining 5.12 feet in 0.8 mile. Overall, it declines 8.71 feet in 0.9 mile between 10104 and 10092. This indicates local ground-water flow to the northwest. The higher water level and slightly poorer water quality found in the vicinity of test hole No. 10104 relative to that found near No. 10100 may be a result of influence from the Fort Union Group.

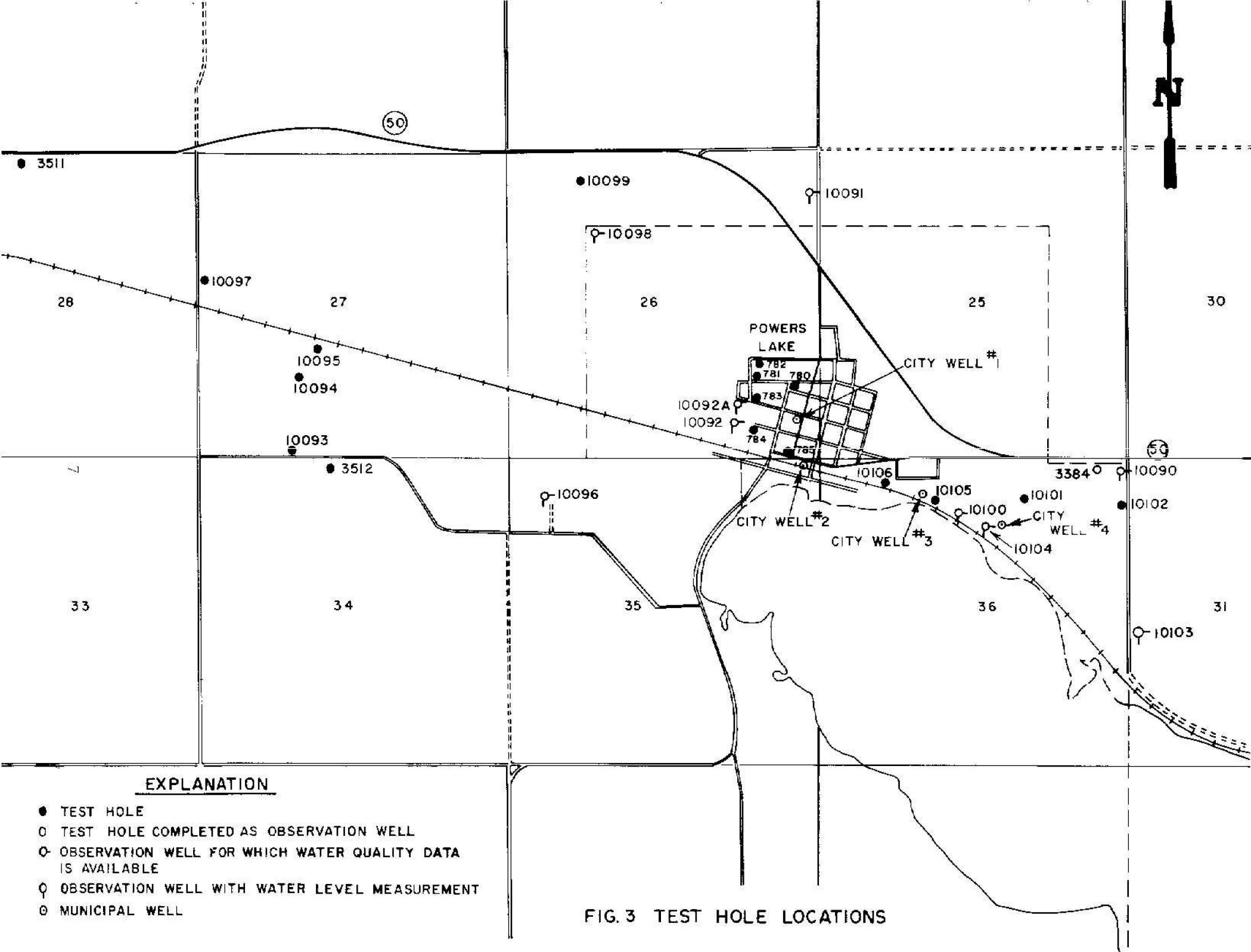


FIG. 3 TEST HOLE LOCATIONS

The aquifer material in 10104 is separated from bedrock by only a thin layer of clay whereas the aquifer material found in 10100 is separated from bedrock influences by 67 feet of glacial till and fluvial clay. It is also possible that, given the discontinuous and lenticular nature of the fluvial deposits in the White Lake depression, the units that have been screened in the three observation wells have no or very little hydrologic connection. This is most probably the case with test hole No. 10092, it being completed in an entirely different unit from holes 10100 and 10104.

The chemical analysis of the water is shown in table 2 and an explanation of the significance of each constituent is given in table 3. It is highly likely that the Shell Creek aquifer system receives the majority of its recharge from the Fort Union Formation (Armstrong, 1971) which influences the water quality and also increases the hydrostatic head (Paulson, 1954). The best overall water quality occurs in the vicinity of observation well No. 10100. Analysis of water obtained from this observation well indicates a concentration of total dissolved solids of 863 mg/l. This value is the lowest determined from samples from the three observation wells. The hardness, sodium, sulfate, and iron concentrations are 450 mg/l, 160 mg/l, 290 mg/l, and .02 mg/l, respectively. The hardness is the highest and the other values are the lowest occurring among the three observation wells. Hardness decreases and dissolved solids, sodium, sulfate, and iron concentrations increase with distance from observation well No. 10100. This is displayed in the analysis of water obtained from observation wells No. 10104 and 10092. The water obtained from No. 10092 had a total dissolved solids concentration of 1380 mg/l. The hardness, sodium, sulfate, and iron concentrations were 110 mg/l, 440 mg/l, 450 mg/l, and .45 mg/l, respectively. Increased hardness

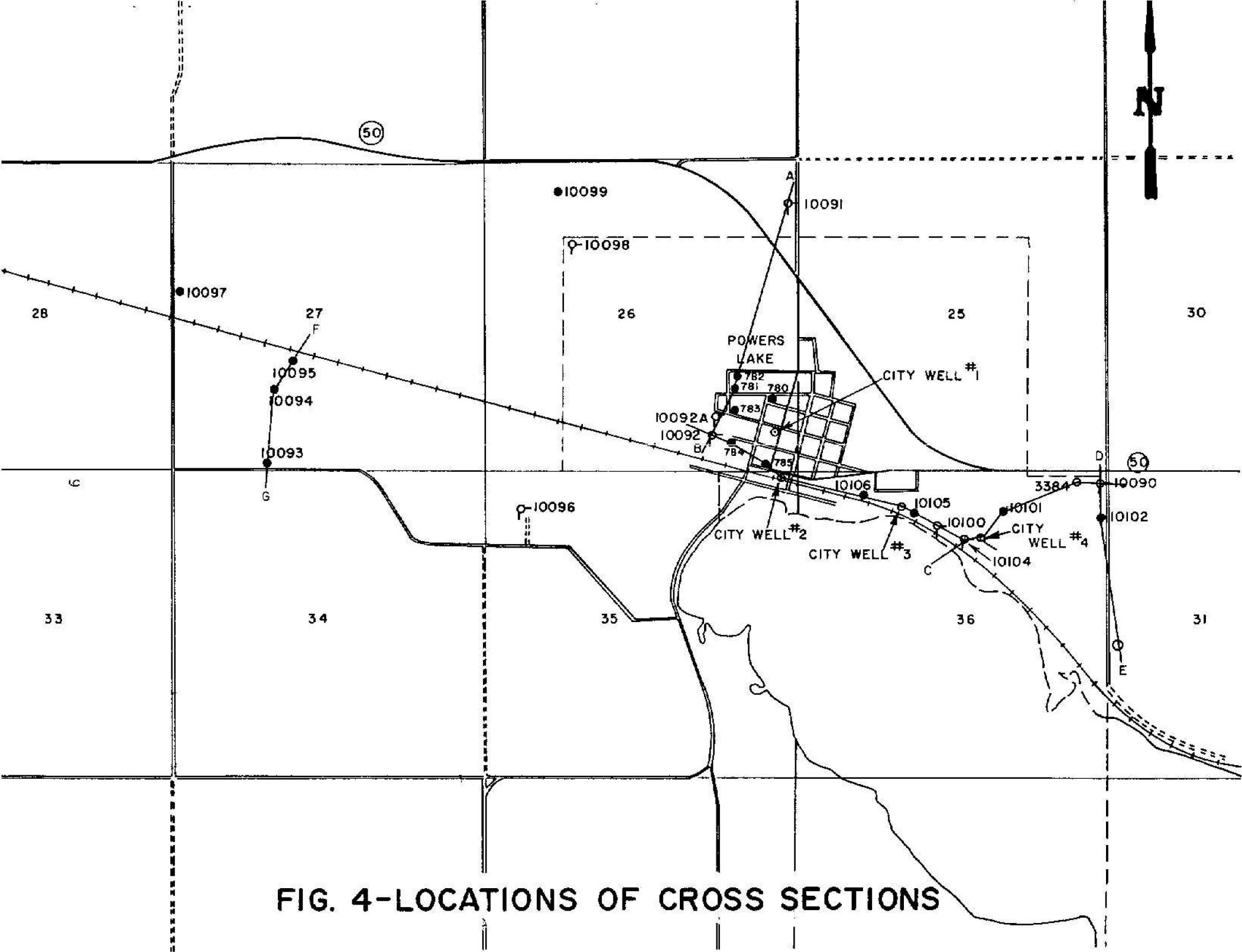


FIG. 4-LOCATIONS OF CROSS SECTIONS

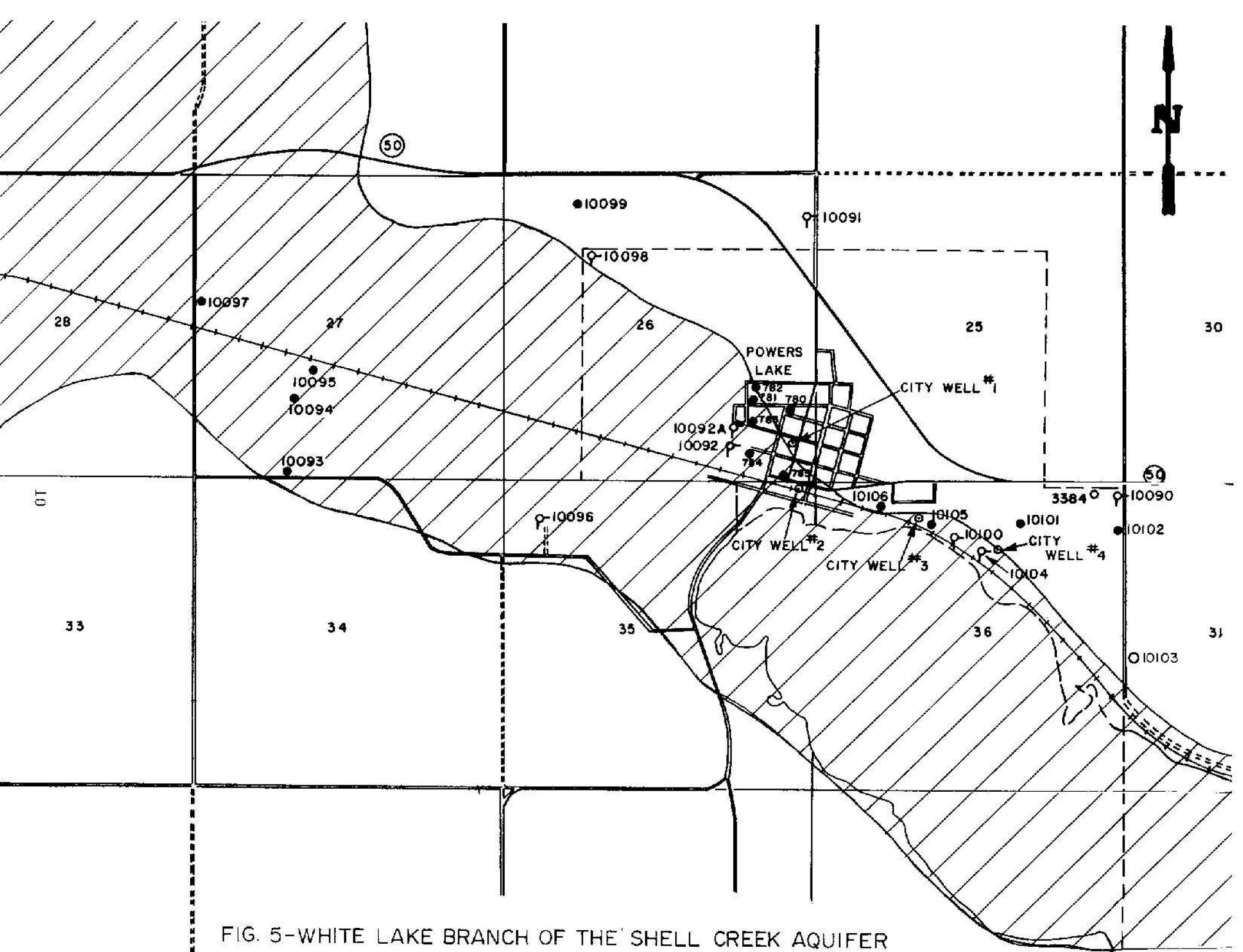


FIG. 5-WHITE LAKE BRANCH OF THE SHELL CREEK AQUIFER

and decreased sodium concentrations near 10100 may indicate local variations in the flow system and lithologies.

Outwash

A second glacial aquifer present in the area is composed of buried outwash. Its boundary is shown in fig. 6. It occurs at an elevation from 2150 to 2200+ feet above msl and may be bounded generally by the 2200 foot elevation in the wall of the White Earth River valley and White Lake depression (fig. 4 and plate 1). Test holes 780, 781, 782, 783, 785, 10090, 10091, 10092A, 10098, 10099, 10101, 10102, 10103, 10106, and 3384, and possibly city wells 1 and 2 have penetrated it. Test holes 10090, 10091, 10092A, 10098, and 10103 were completed as observation wells. The aquifer ranges from 15 to 50 feet thick. Depth to the aquifer ranges from 0 to 60 feet. It is composed of predominantly rounded, well sorted, medium or coarse sand and fine to medium gravel, where exposed at the surface. Carbonates, detrital shale, and silicates are found in nearly equal proportions. Some finer sands occasionally contain considerable quantities of clay and silt.

The highest water levels are found in the vicinity of observation wells No. 10090 and 10091 at 2208.15 and 2208.37 feet above msl respectively (tables 1 and 2). Lower water levels are found in observation wells No. 10103, 10092A, and 10098 at 2200.23, 2188.74, and 2187.36 feet above msl respectively. Ground water movement is from the higher elevations north and east of Powers Lake toward the White Earth River valley and the White Lake depression.

Relatively better quality is found in the vicinity of observation well No. 10103. Analysis of a sample obtained from the observation well indicates a total dissolved solids concentration of 854 mg/l. The hardness, sodium, sulfate, and iron concentrations are 320 mg/l, 170 mg/l, 170 mg/l, and .08 mg/l,

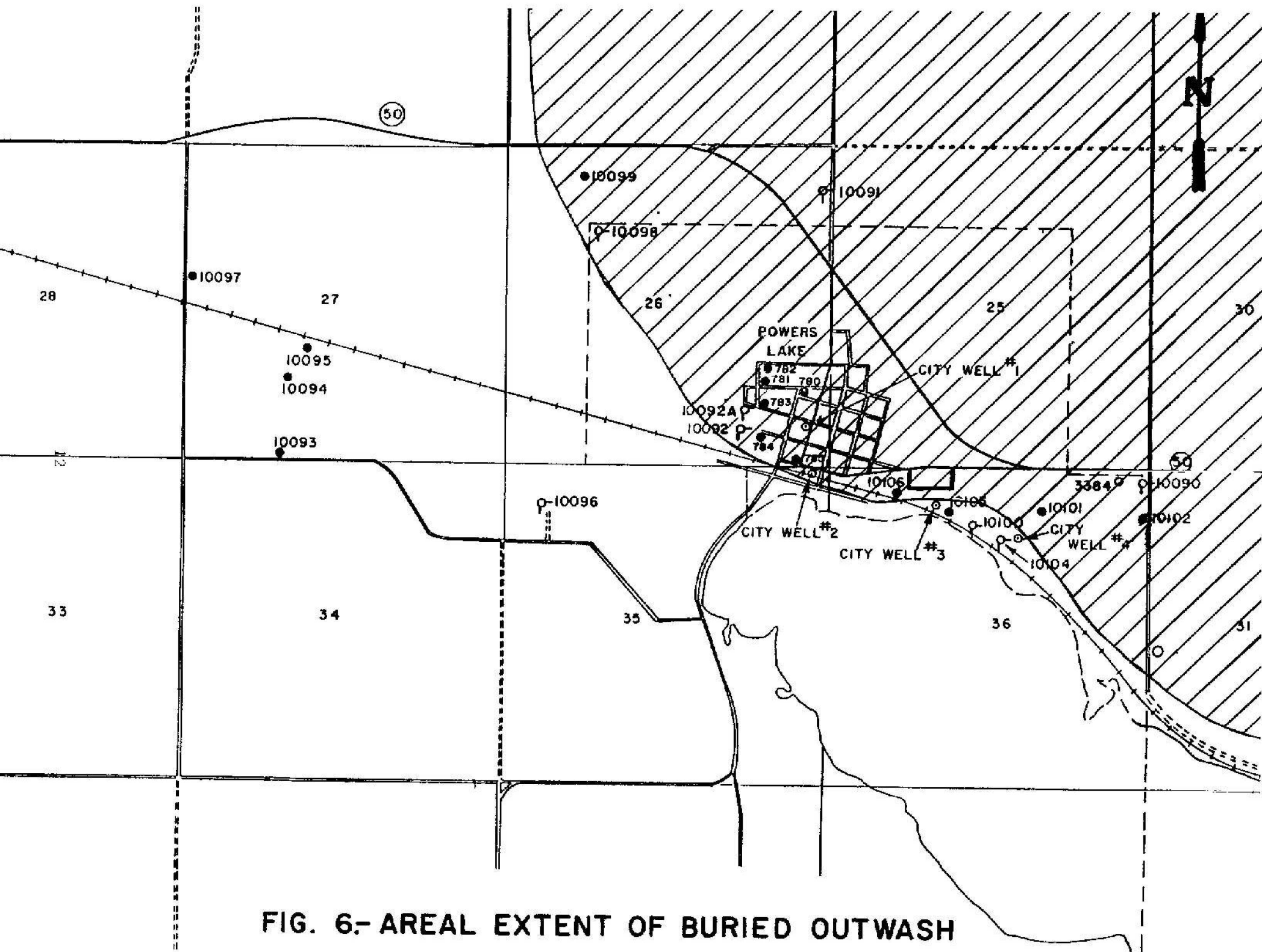


FIG. 6.- AREAL EXTENT OF BURIED OUTWASH

respectively. The poorest quality water is found in the vicinity of city well No. 1. Analysis of a sample obtained from this well indicates a concentration of total dissolved solids of 1480 mg/l. Hardness, sodium, sulfate, and iron concentrations are 320 mg/l, 430 mg/l, 530 mg/l, and 1.7 mg/l, respectively.

The existence of two distinct aquifers is inferred from the test hole logs and cross sections. The degree of connection between the units is not known. Water levels vary only slightly between the units. Observation wells No. 10092 and 10092A have been completed in the White Lake Branch and the outwash with water levels of 2187.2 and 2188.74 feet above msl, respectively. It is unlikely that the two units are connected, the valley-ward flow in the upper unit intersecting the White Lake Branch aquifer and contributing to its northwesterly flow.

Summary

Test drilling revealed the presences of two aquifers in the area. They are the fluvial sands and gravels deposited in the White Lake depression and glacial outwash found in the higher elevations north of the city of Powers Lake. The deposits of the White Lake depression possess a greater saturated thickness and slightly superior water quality. Within the White Lake depression, deposits possessing relatively better quality water and higher water levels were encountered at the southeast corner of the city along the railroad tracks. The two new city wells (wells No. 3 and 4), were completed in these deposits.

Table 1 - Logs of Test Holes

The following test hole logs are compiled data of geologist's sample descriptions, driller's logs, and geophysical logs which include resistance and spontaneous potential. Grain-size classification throughout this report uses K. C. Wentworth's scale from Compton (1967). Color descriptions are of wet samples and are based upon color standards of the national research council (Goddard, et.al., 1948). Test holes completed as observation wells have surveyed elevations, all others are inferred from topographic maps published by the U. S. Geological Survey. Observation wells are composed of 1½" pvc plastic casing and screened bottoms. Well depths and screened producing intervals (S.I.) are also noted.

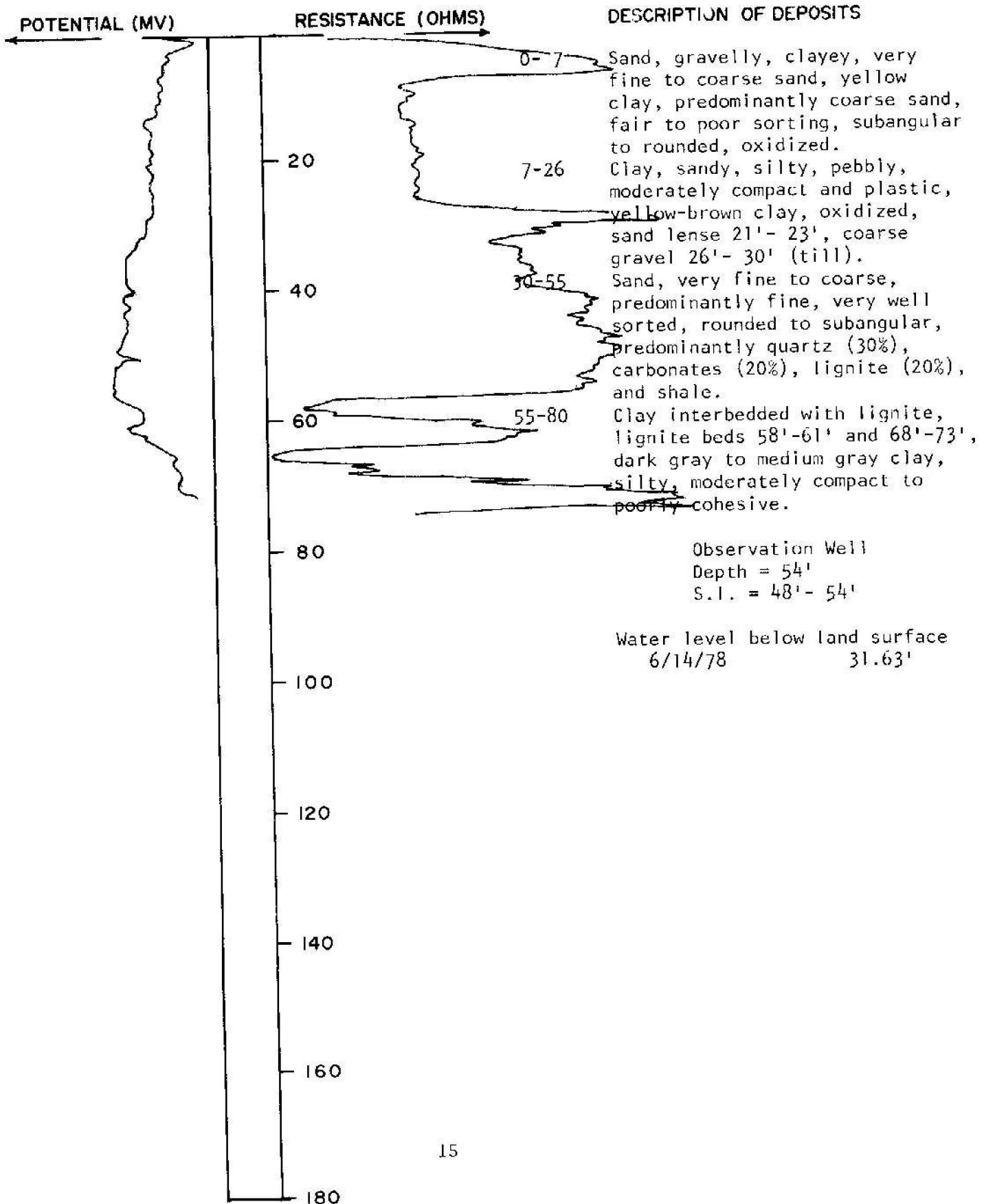
TEST HOLE 10091

LOCATION: 159-93-26AAD

DATE DRILLED: 6/6/78

ELEVATION: 2240
(FT, MSL)

DEPTH: 80
(FT)



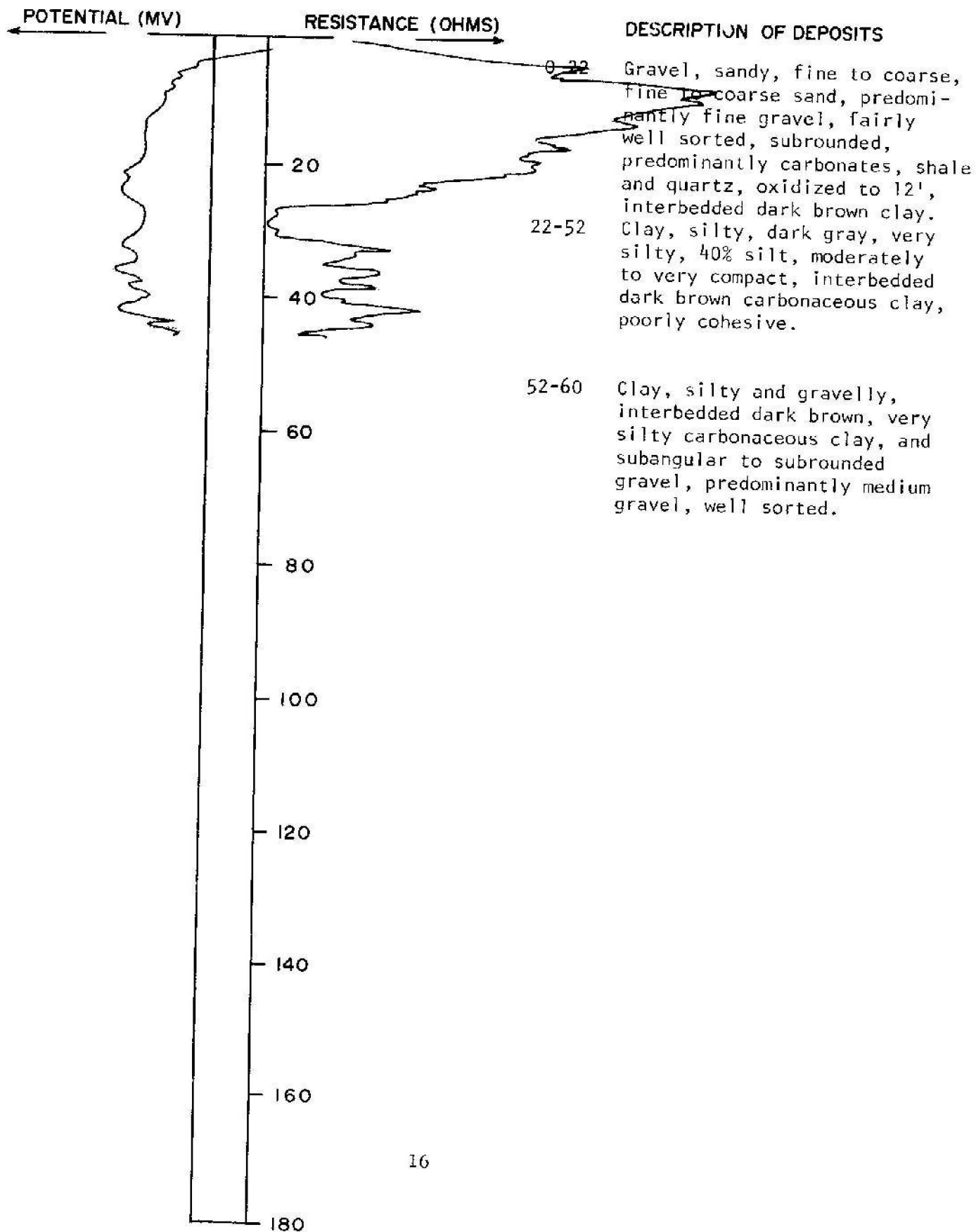
TEST HOLE 10099

LOCATION: 159-93-26BAC

DATE DRILLED: 6/8/78

ELEVATION: 2193
(FT, MSL)

DEPTH: 60
(FT)



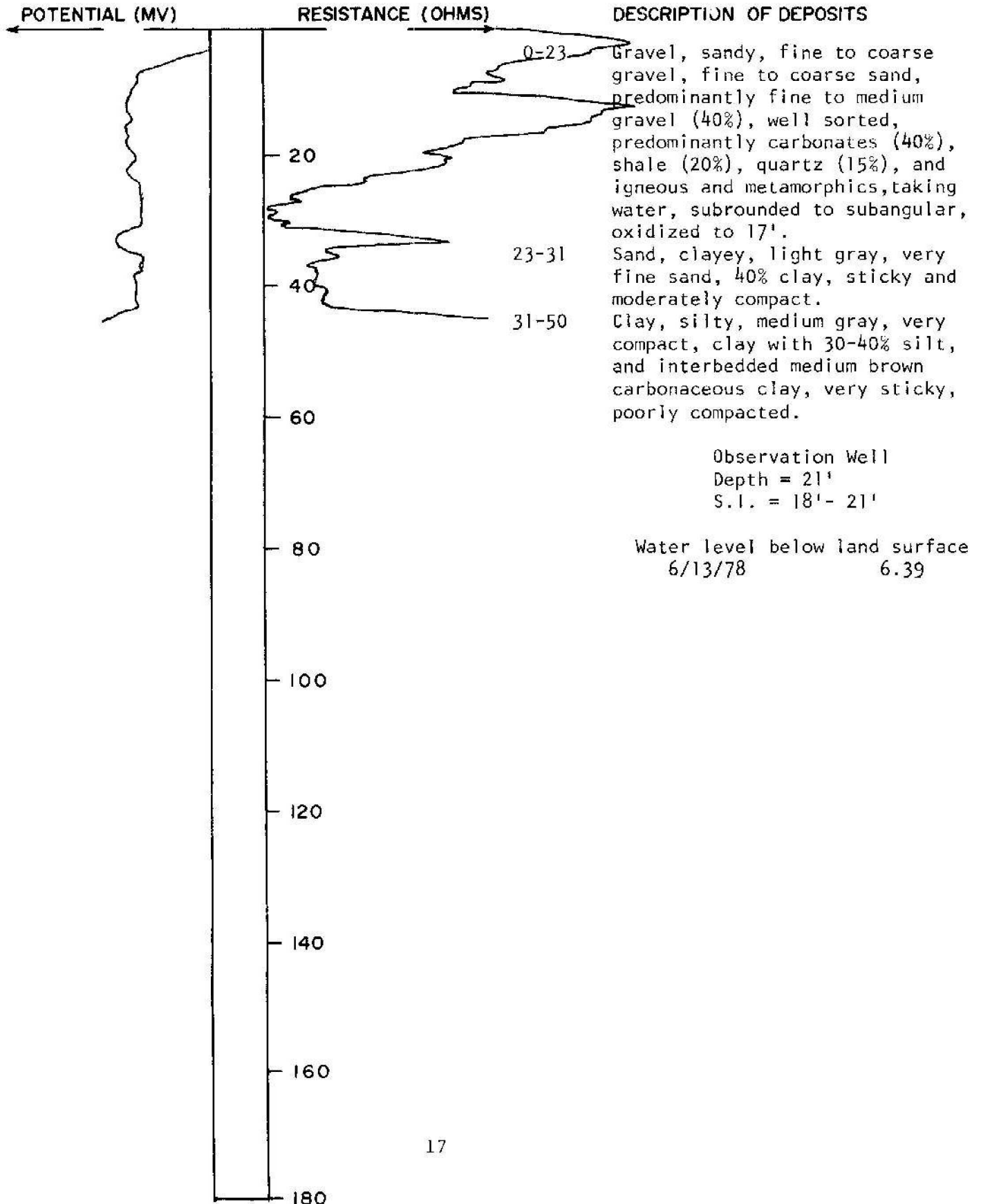
TEST HOLE 10098

LOCATION: 159-93-26BDB

DATE DRILLED: 6/8/78

ELEVATION: 2192
(FT, MSL)

DEPTH: 50
(FT)



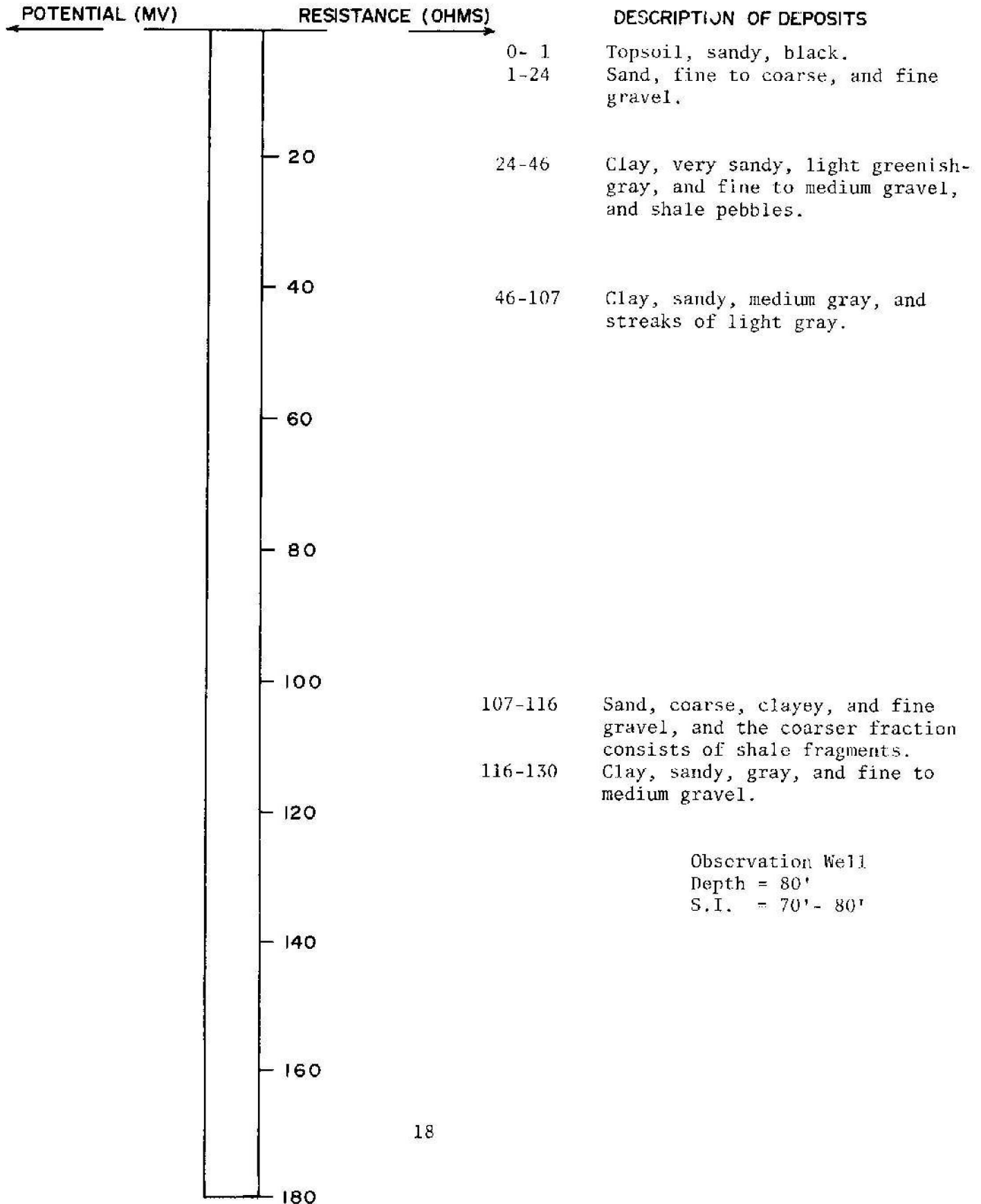
TEST HOLE 781

LOCATION: 159-093-26DAB

DATE DRILLED:

ELEVATION:
(FT, MSL)

DEPTH: 130
(FT)



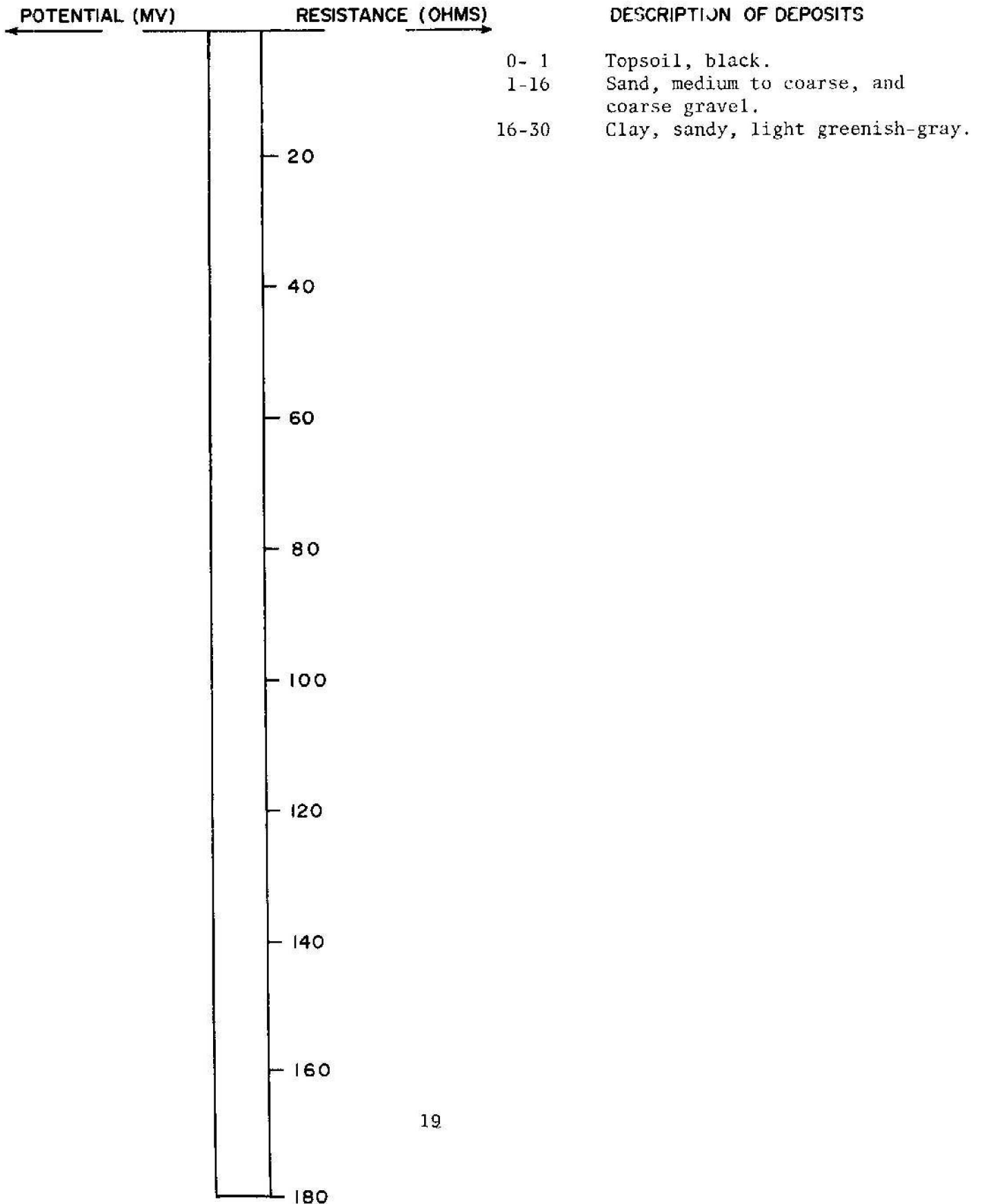
TEST HOLE 782

LOCATION: 159-093-26DAC

DATE DRILLED:

ELEVATION:
(FT, MSL)

DEPTH: 30
(FT)



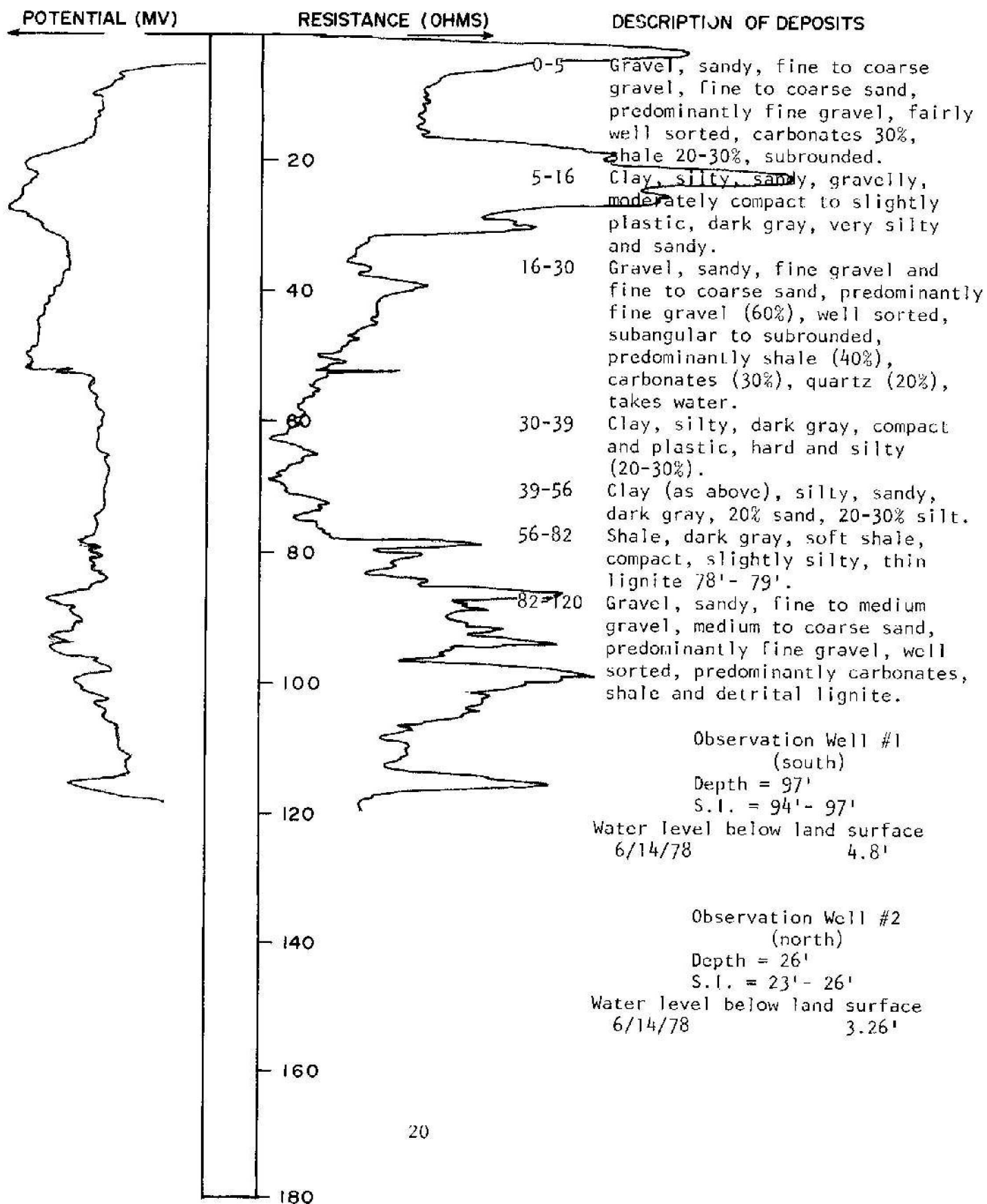
TEST HOLE 10092

LOCATION: 159-93-26DDA₁ and 2

DATE DRILLED: 6/6/78

ELEVATION: 2192
(FT, MSL)

DEPTH: 120
(FT)



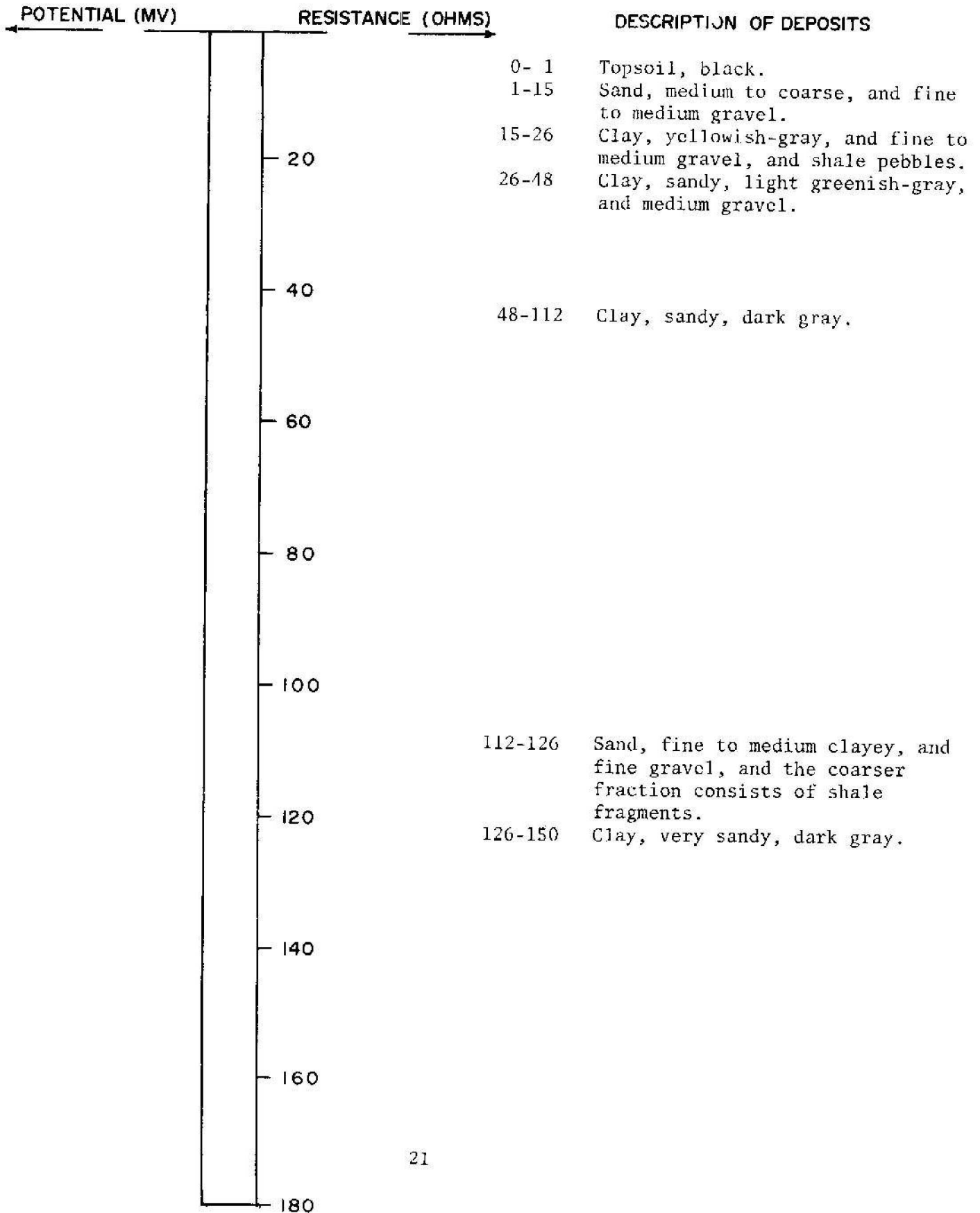
TEST HOLE 780

LOCATION: 159-093-26DDA

DATE DRILLED:

ELEVATION:
(FT, MSL)

DEPTH: 150
(FT)



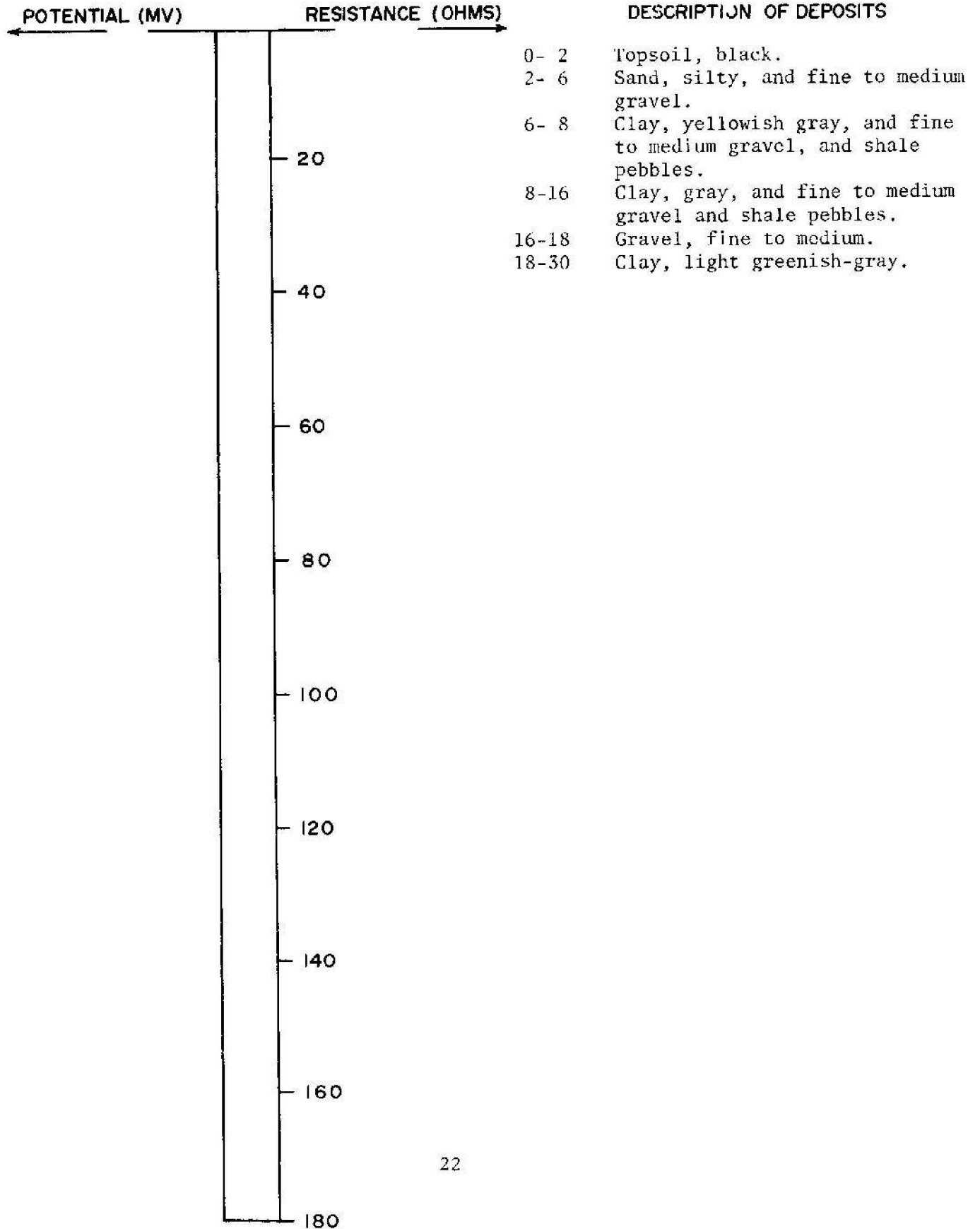
TEST HOLE 783

LOCATION: 159-093-26DDB

DATE DRILLED:

ELEVATION:
(FT, MSL)

DEPTH: 30
(FT)



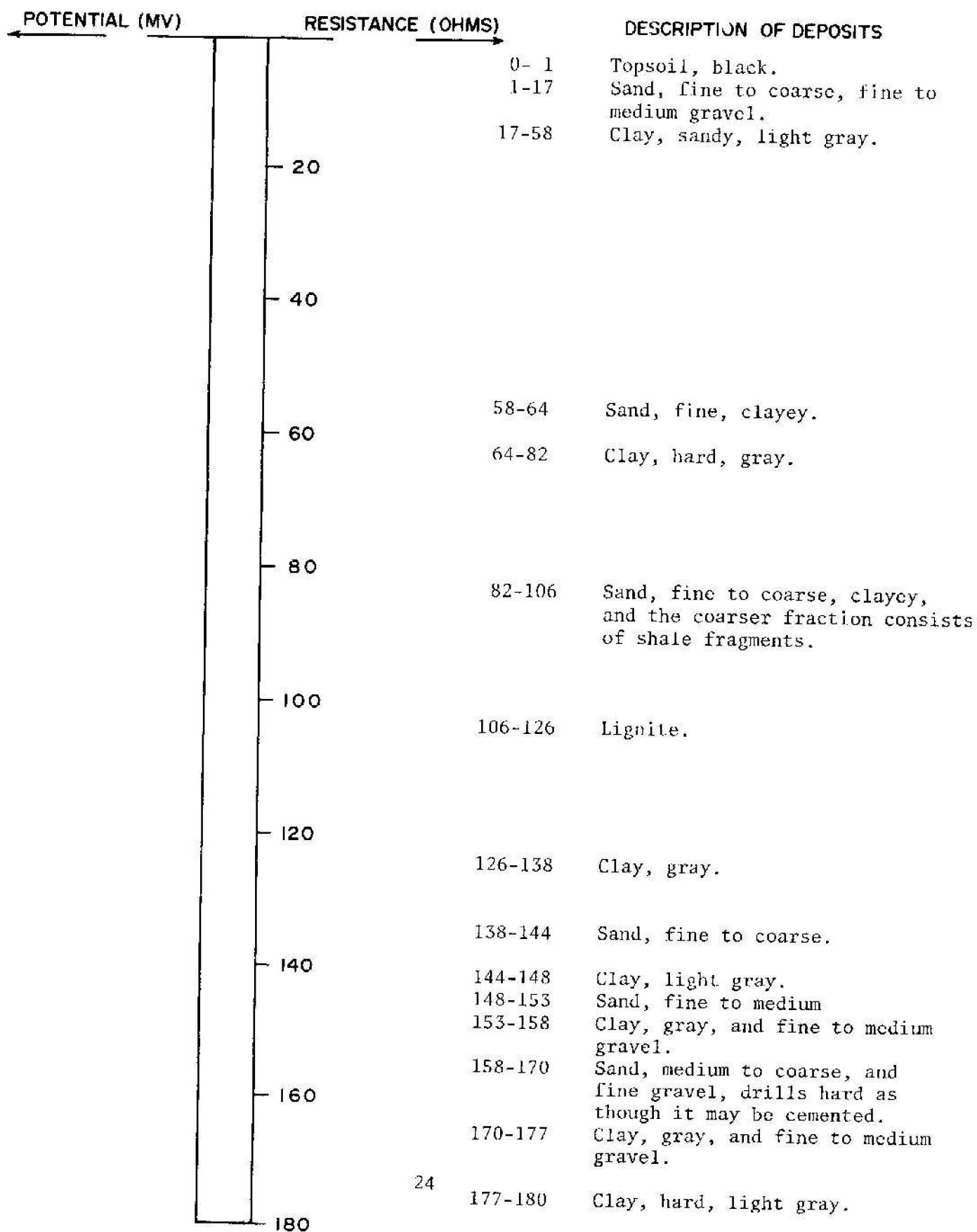
TEST HOLE 785

LOCATION: 159-093-26DDD

DATE DRILLED:

ELEVATION:
(FT, MSL)

DEPTH: 180
(FT)



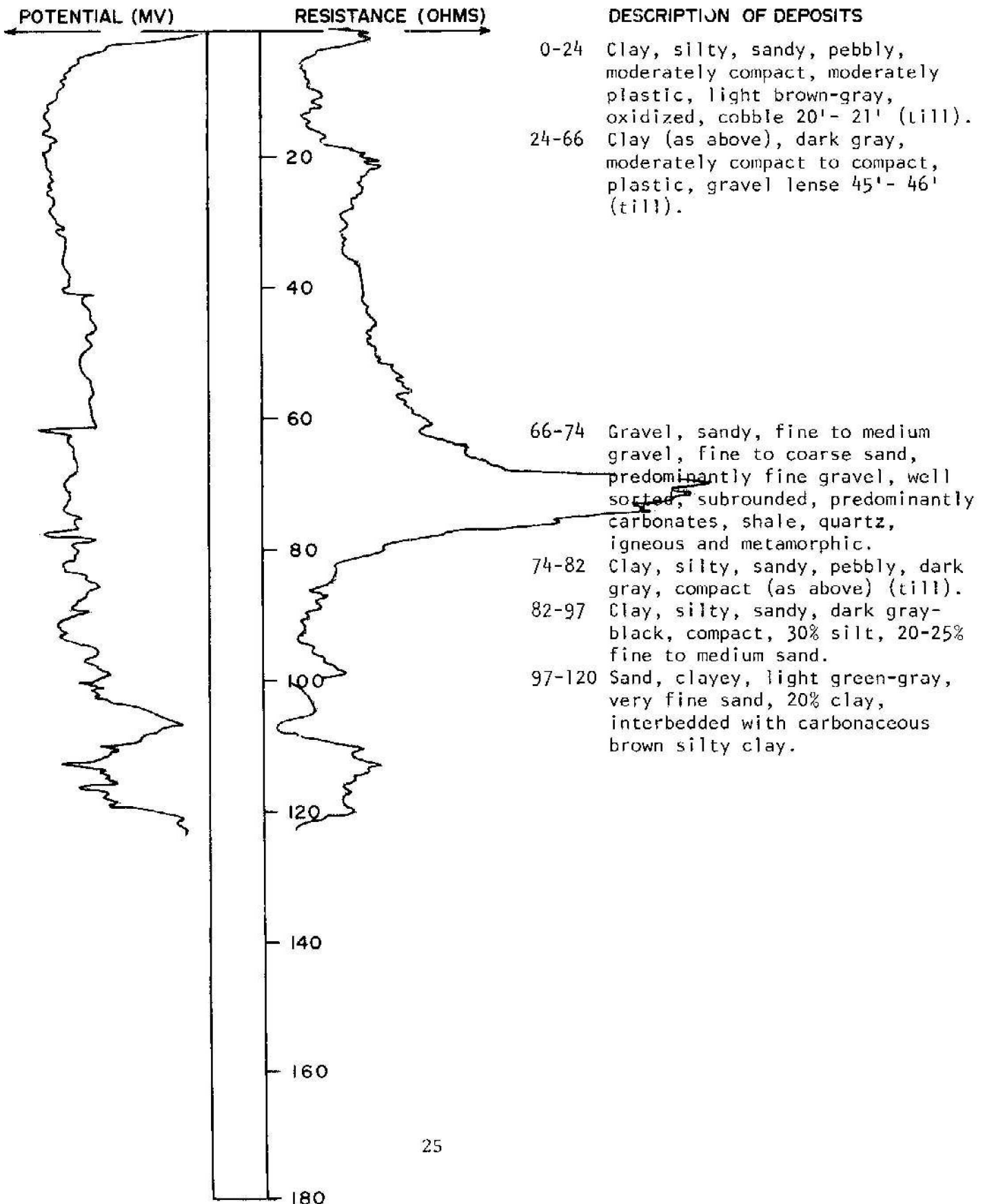
TEST HOLE 10097

LOCATION: 159-93-27BCC

DATE DRILLED: 6/8/78

ELEVATION: 2212
(FT, MSL)

DEPTH: 120
(FT)



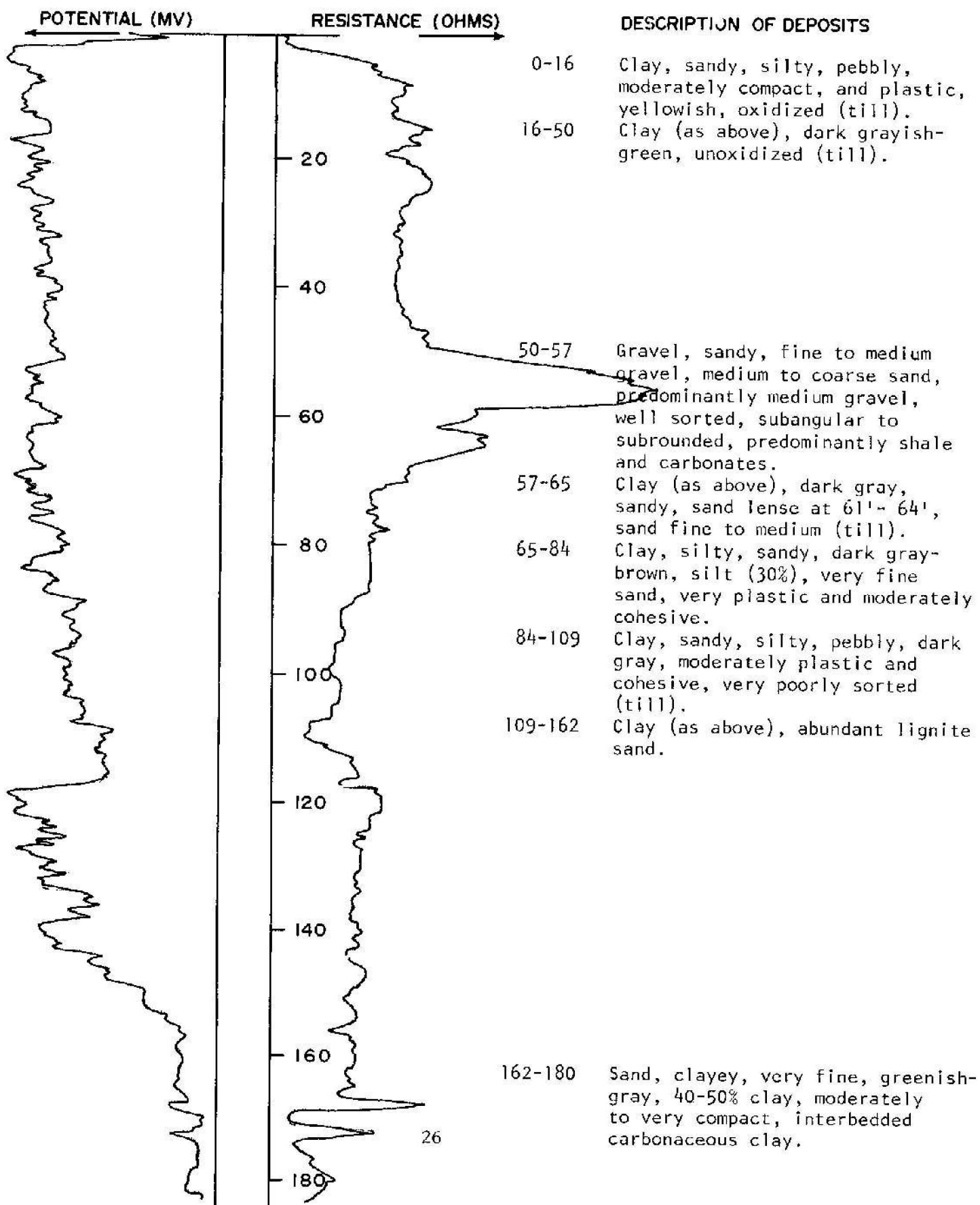
TEST HOLE 10095

LOCATION: 159-93-27CAA

DATE DRILLED: 6/7/78

ELEVATION: 2192
(FT, MSL)

DEPTH: 180
(FT)



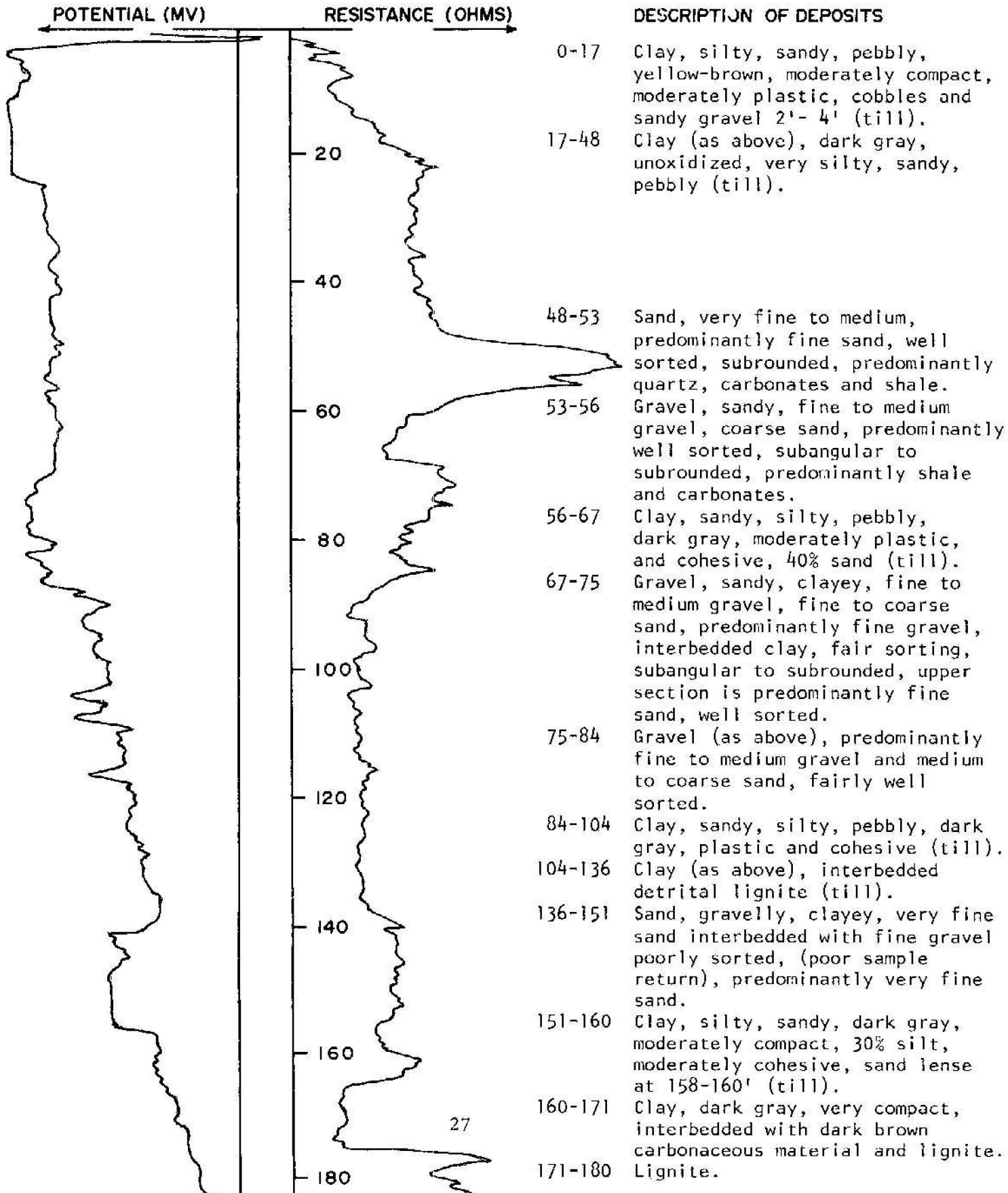
TEST HOLE 10094

LOCATION: 159-93-27CAC

DATE DRILLED: 6/7/78

ELEVATION: 2190
(FT, MSL)

DEPTH: 180
(FT)



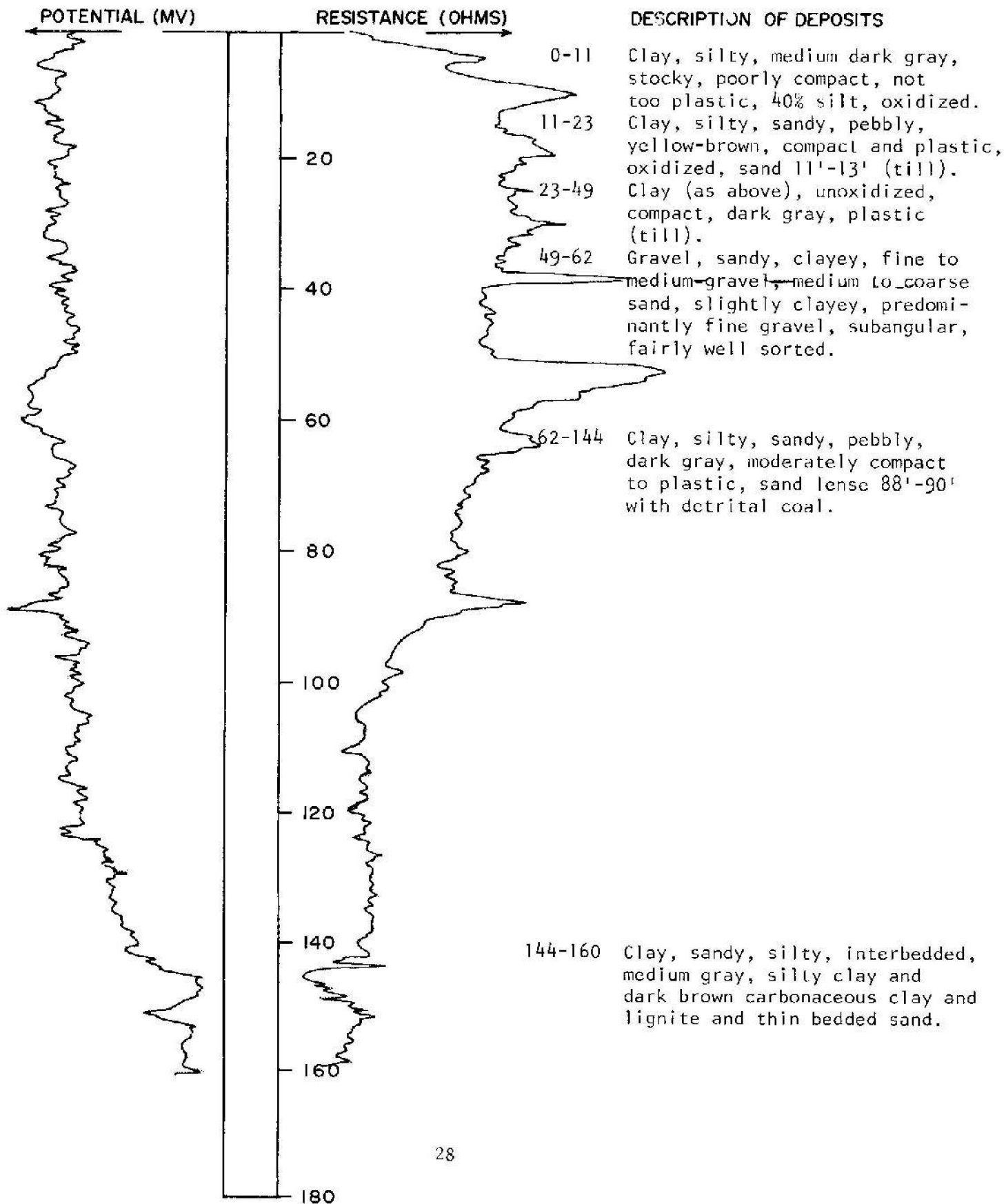
TEST HOLE 10093

LOCATION: 159-93-27CDC

DATE DRILLED: 6/7/78

ELEVATION: 2202
(FT, MSL)

DEPTH: 160
(FT)



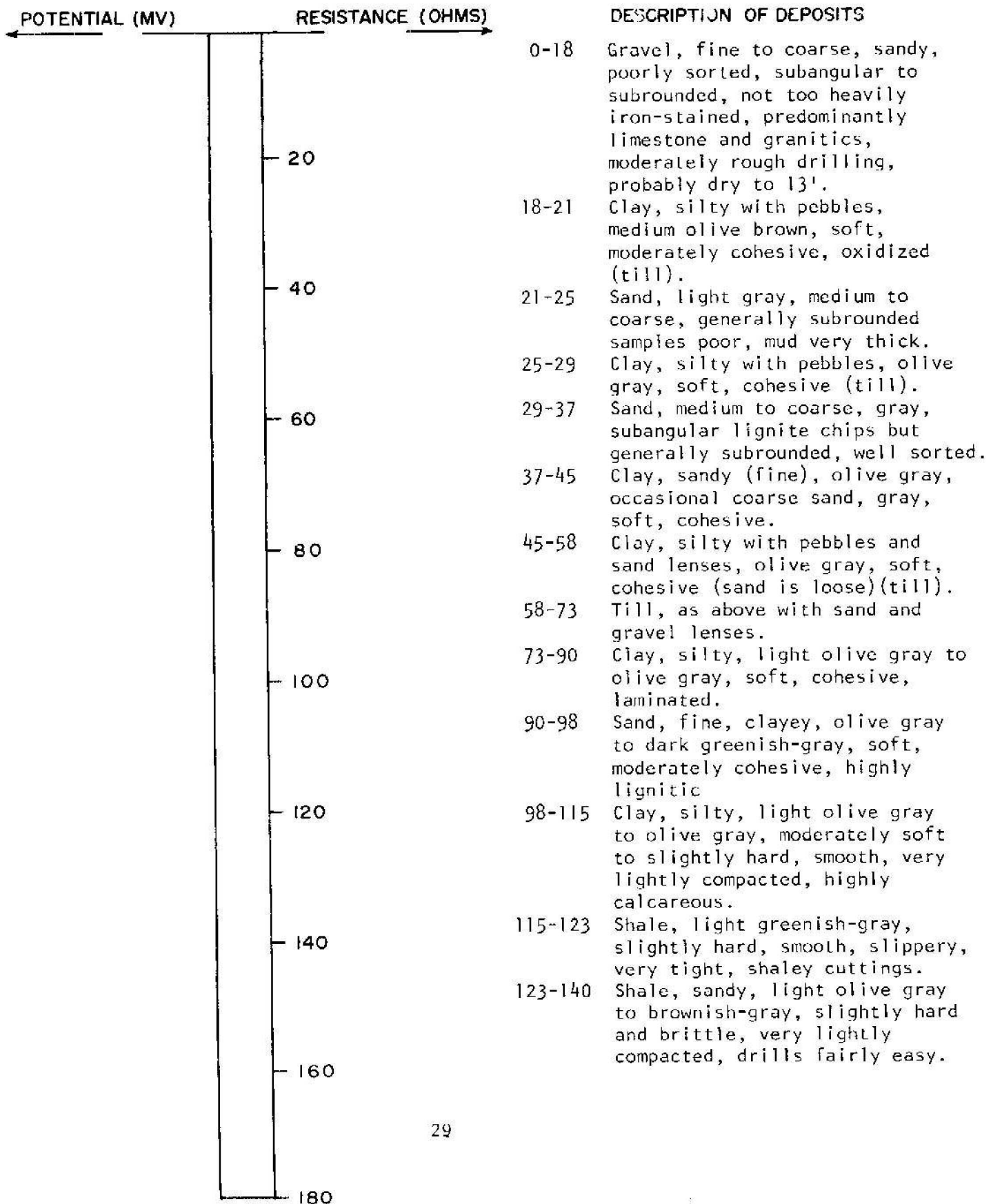
TEST HOLE 3511

LOCATION: 159-93-28BAA

DATE DRILLED: 7/31/67

ELEVATION: 2200
(FT, MSL)

DEPTH: 140
(FT)



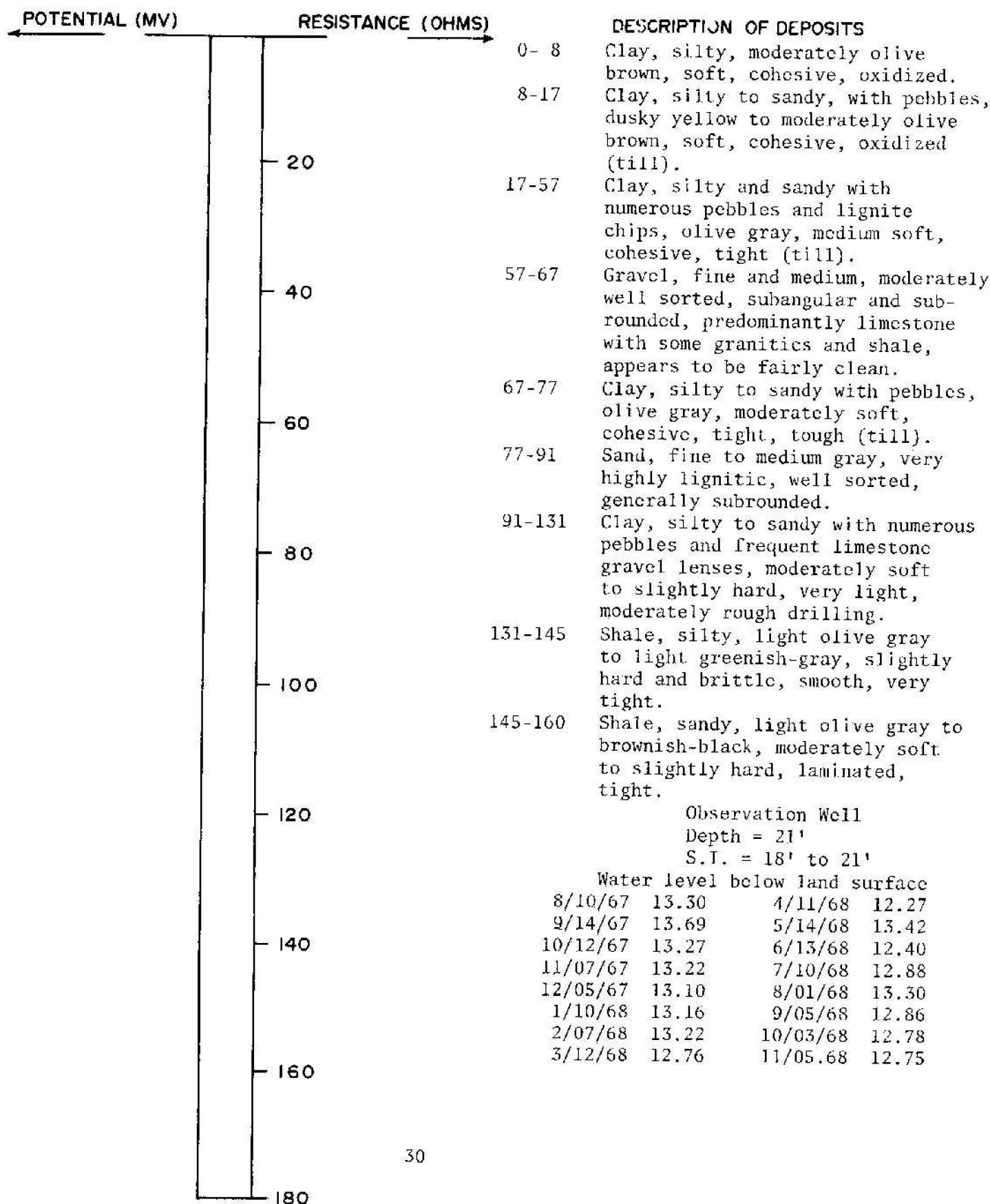
TEST HOLE 3512

LOCATION: 159-93-34BA

DATE DRILLED: 7/31/67

ELEVATION: 2203
(FT, MSL)

DEPTH: 160
(FT)



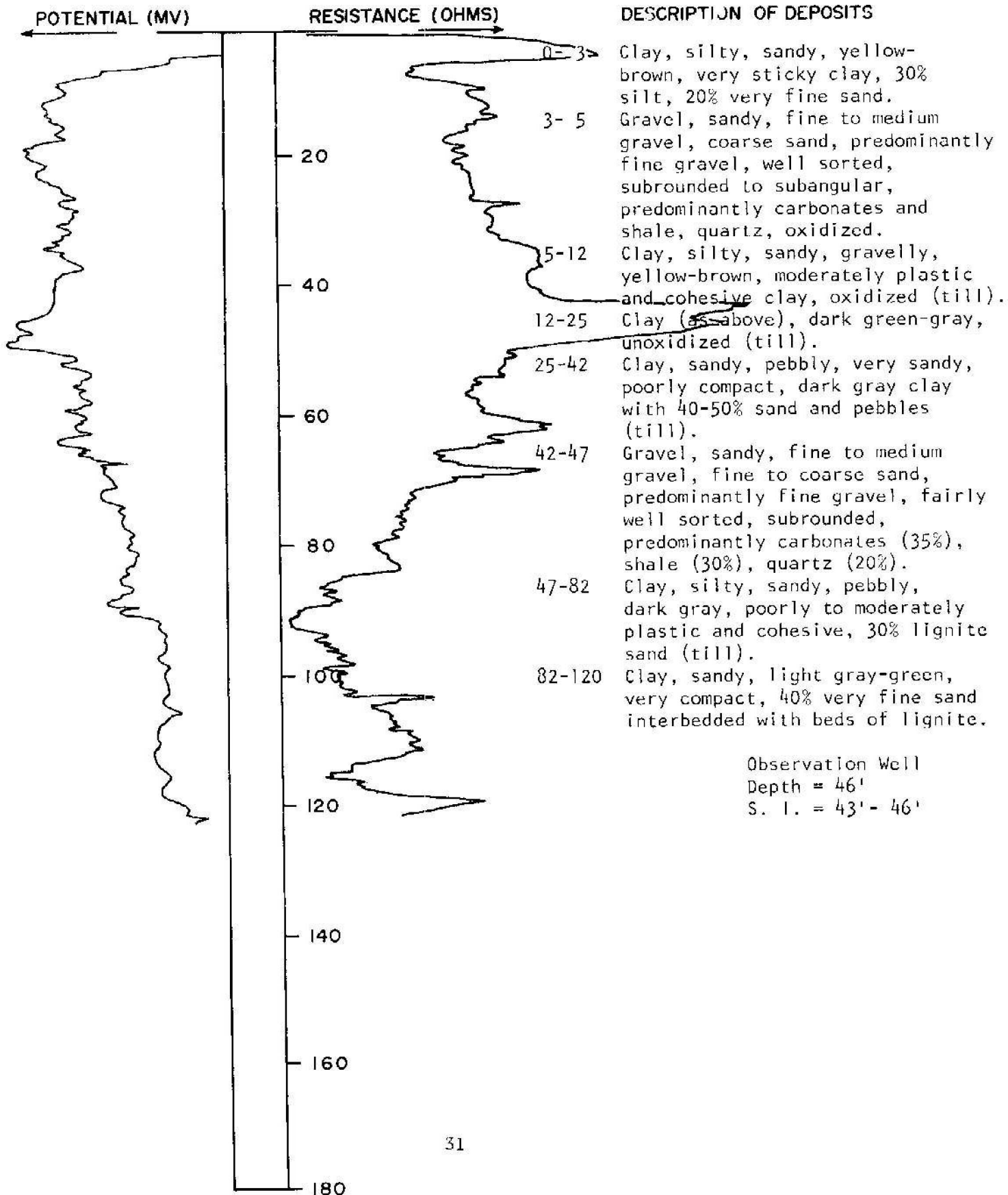
TEST HOLE 10096

LOCATION: 159-93-35bbd

DATE DRILLED: 6/7/78

ELEVATION: 2189
(FT, MSL)

DEPTH: 120
(FT)



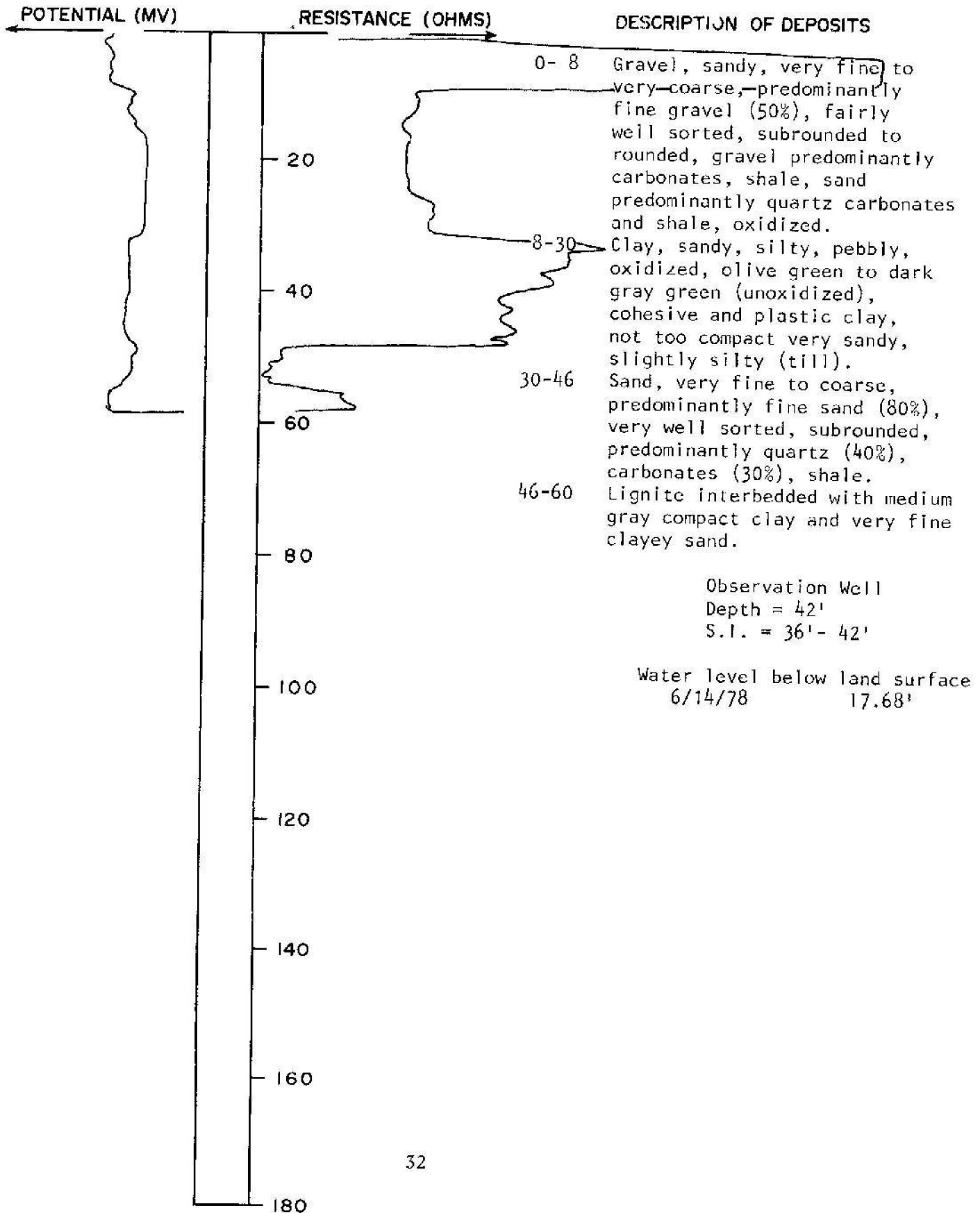
TEST HOLE 10103

LOCATION: 159-92-31CBB

DATE DRILLED: 6-13-78

ELEVATION: 2216
(FT, MSL)

DEPTH: 60'
(FT)



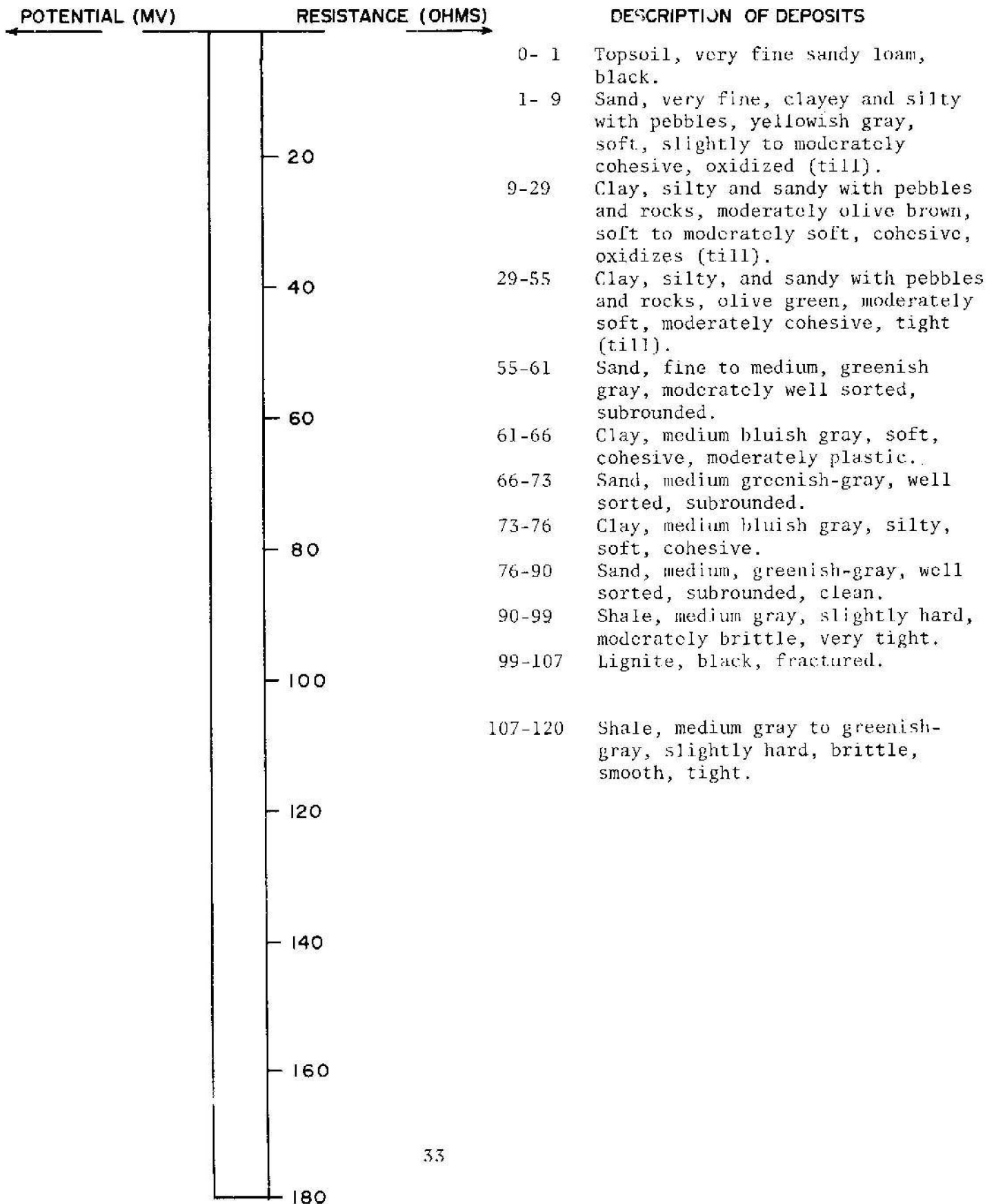
TEST HOLE 3384

LOCATION: 159-093-36AAA

DATE DRILLED: 8/12/66

ELEVATION: 2258
(FT, MSL)

DEPTH: 120
(FT)



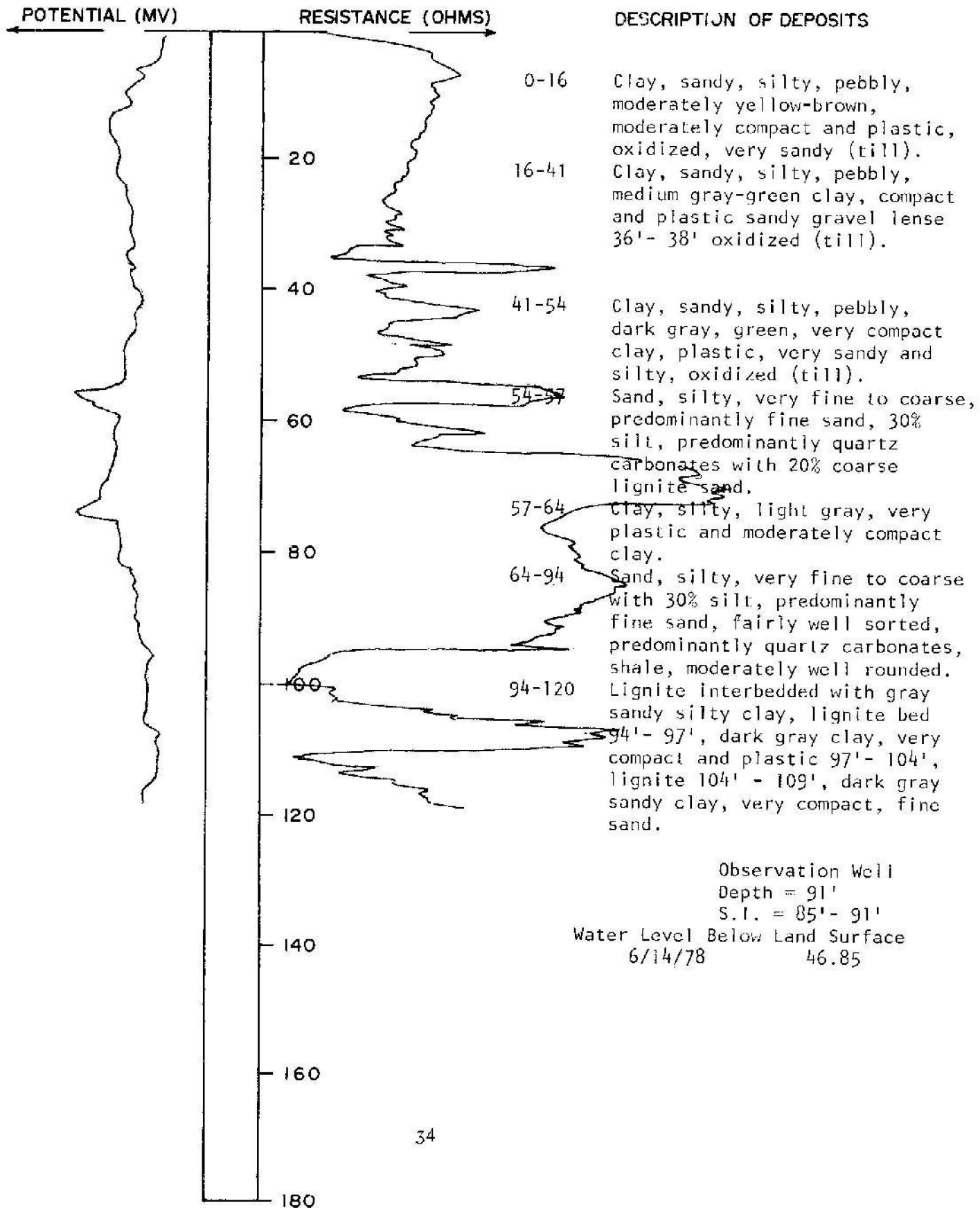
TEST HOLE 10090

LOCATION: 159-93-36AAA₂

DATE DRILLED: 6/6/78

ELEVATION: 2255
(FT, MSL)

DEPTH: 120
(FT)



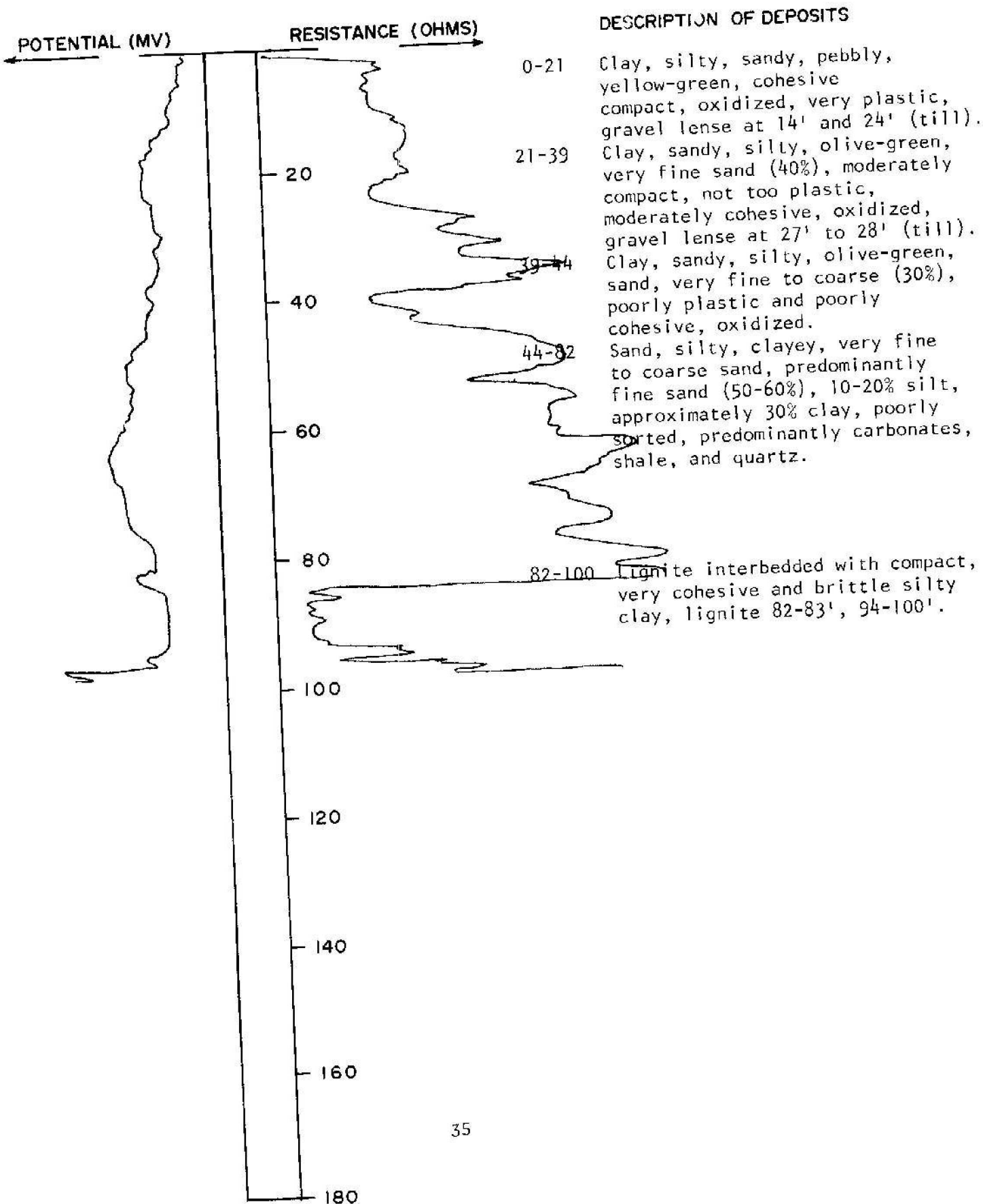
TEST HOLE 10102

DATE DRILLED: 6/13/78

LOCATION: 159-93-36AAD

DEPTH: 100
(FT)

ELEVATION: 2231
(FT, MSL)



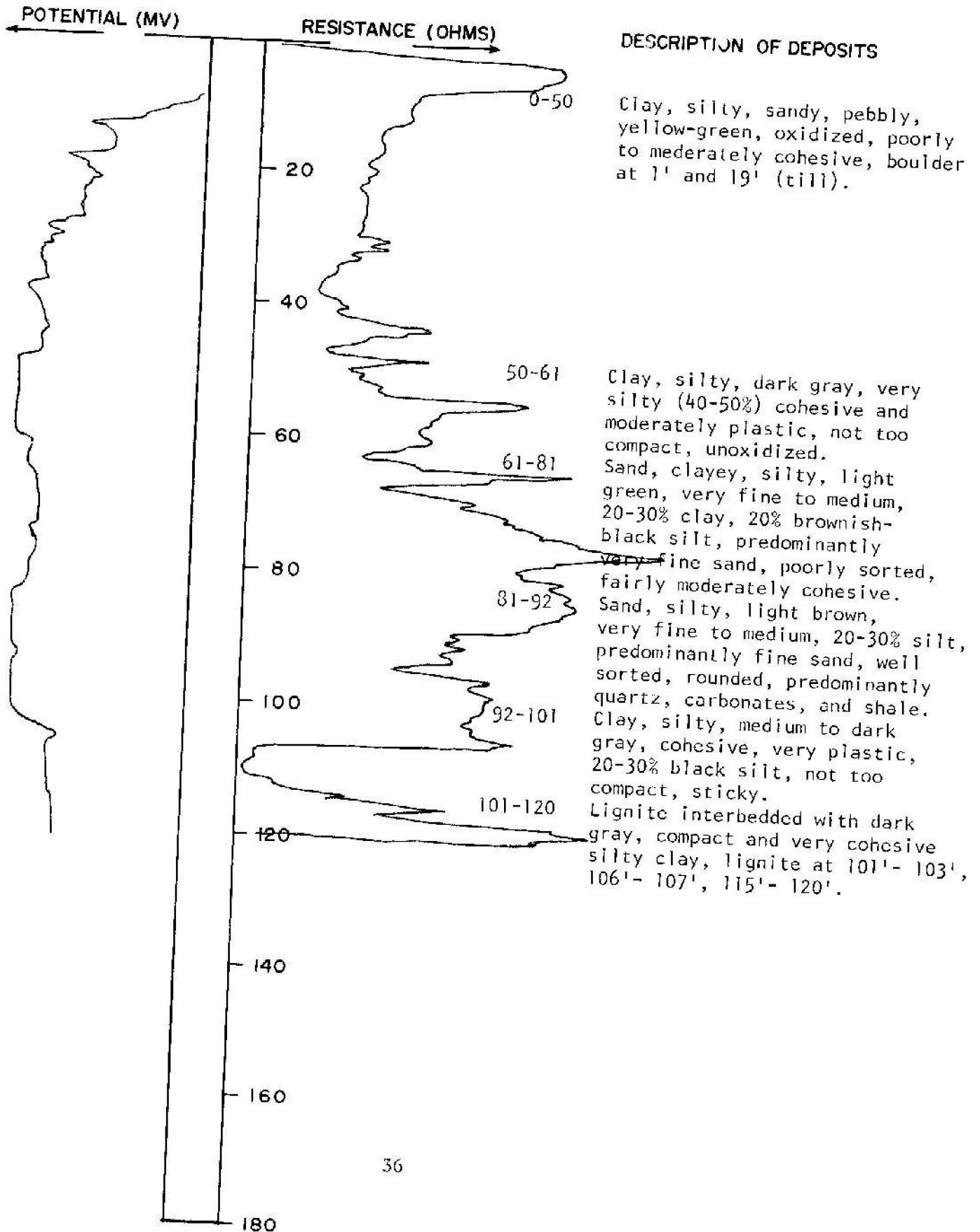
TEST HOLE 10101

LOCATION: 159-93-36ABA

DATE DRILLED: 6-12-78

ELEVATION: 2252
(FT, MSL)

DEPTH: 120
(FT)



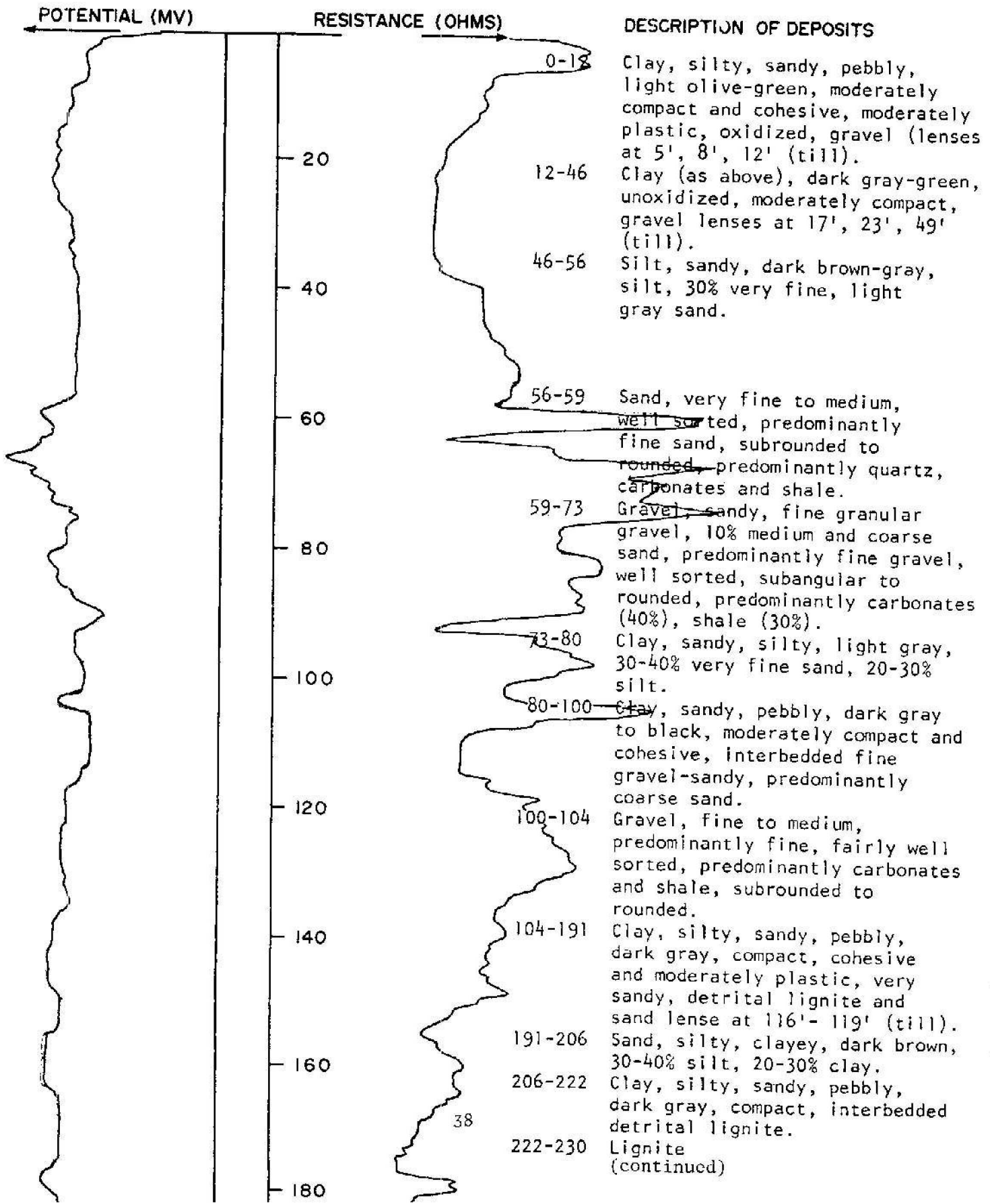
TEST HOLE 10105

LOCATION: 159-93-36BAA

DATE DRILLED: 6/20/78

ELEVATION: 2212
(FT, MSL)

DEPTH: 240
(FT)



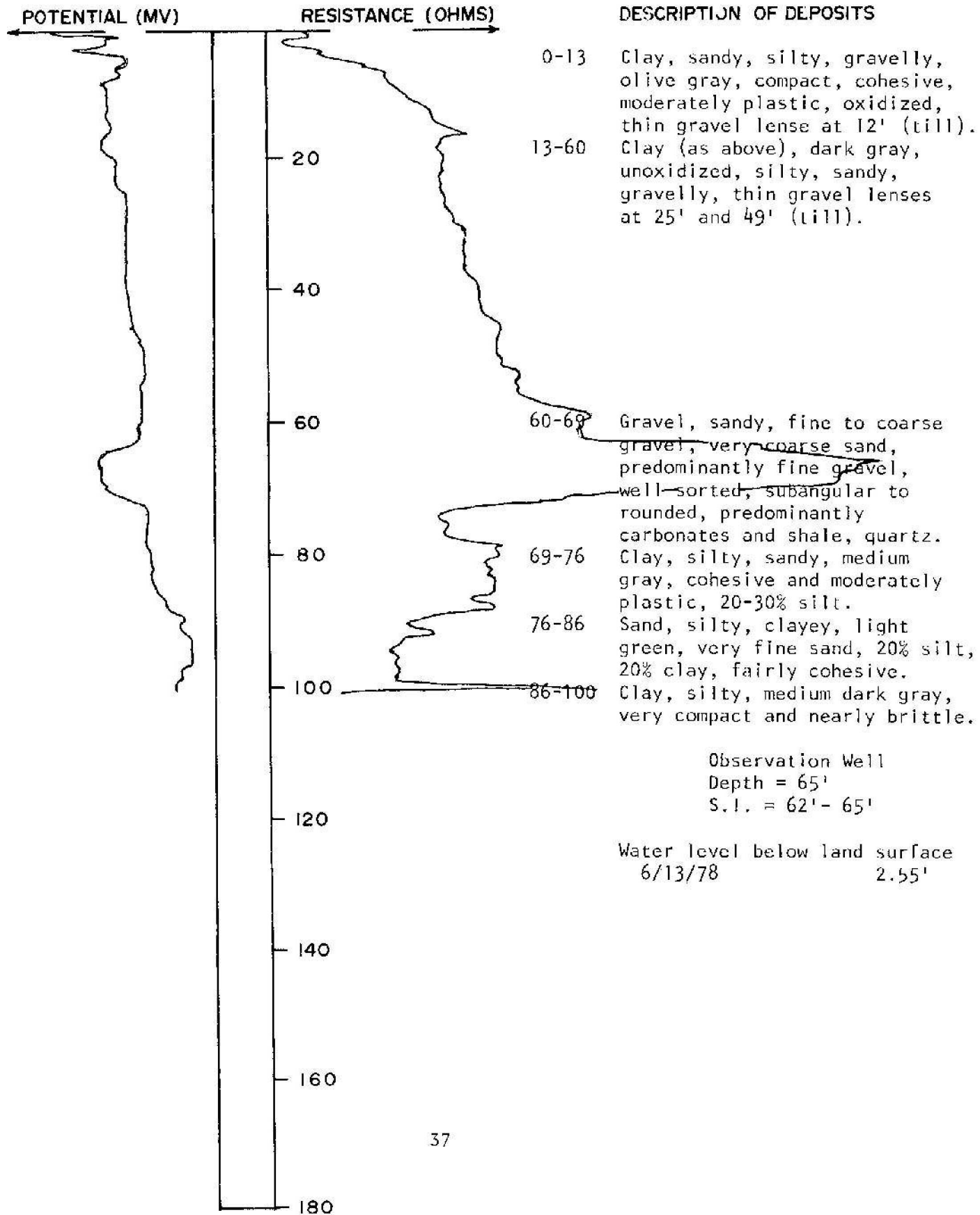
TEST HOLE 10104

LOCATION: 159-93-36ABC

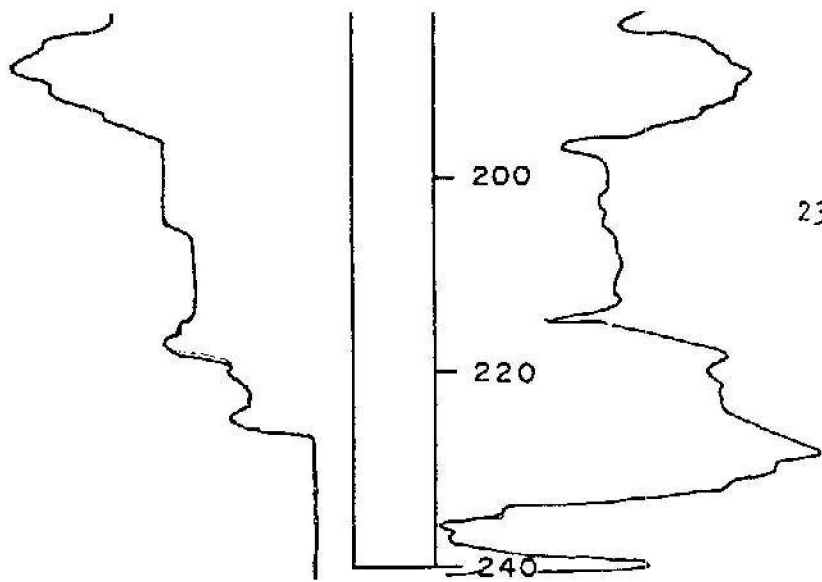
DATE DRILLED: 6/13/78

ELEVATION: 2200
(FT, MSL)

DEPTH: 100
(FT)



10105 continued



230-240 Clay, dark gray, very compact,
and brittle, interbedded lignite.

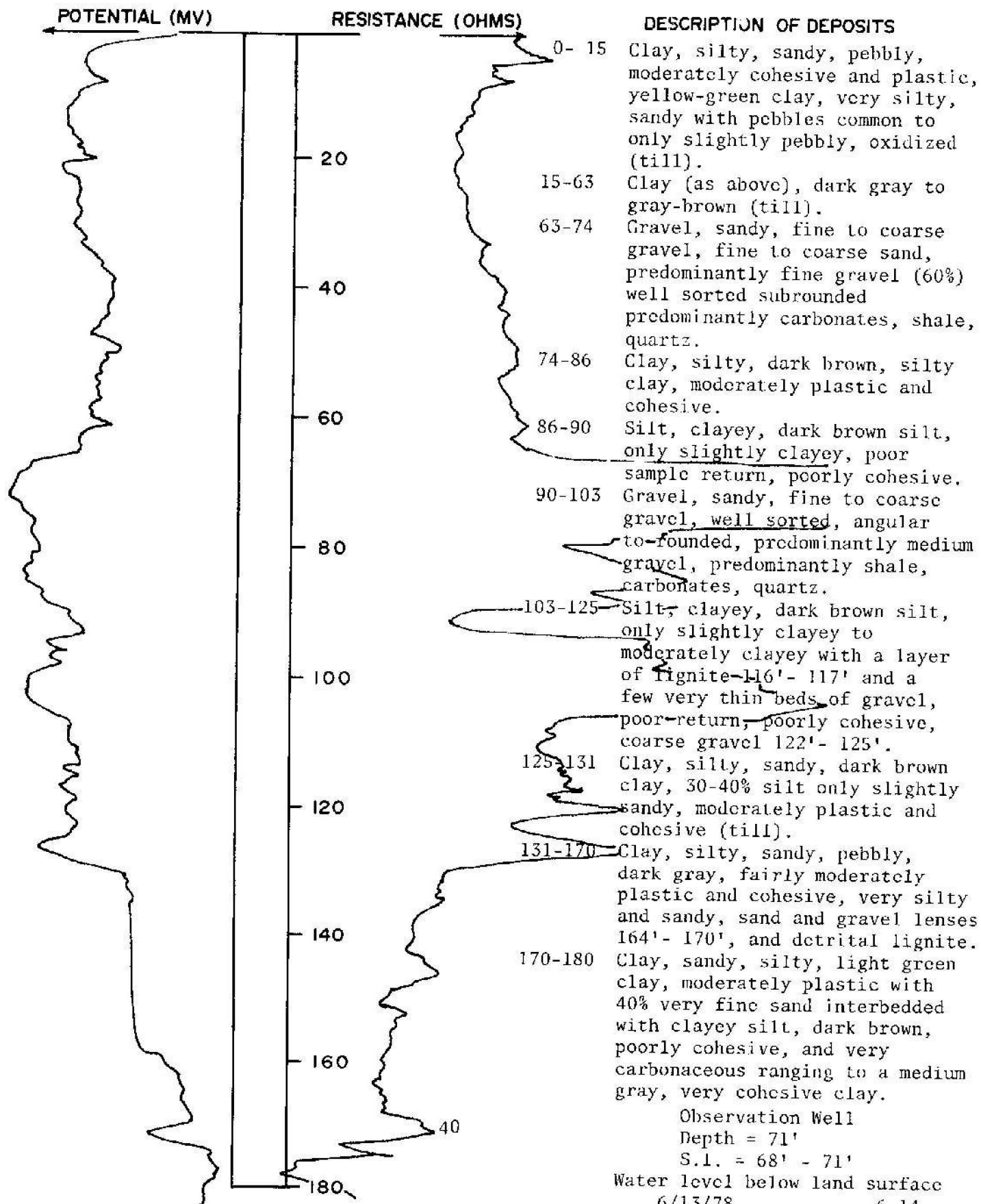
TEST HOLE 10100

LOCATION: 159-93-36BAB

DATE DRILLED: 6/9/78

ELEVATION: 2200
(FT, MSL)

DEPTH: 180'
(FT)



TEST HOLE 10106

LOCATION: 159-93-368BA

DATE DRILLED: 6/20/78

ELEVATION: 2217
(FT, MSL)

DEPTH: 80
(FT)

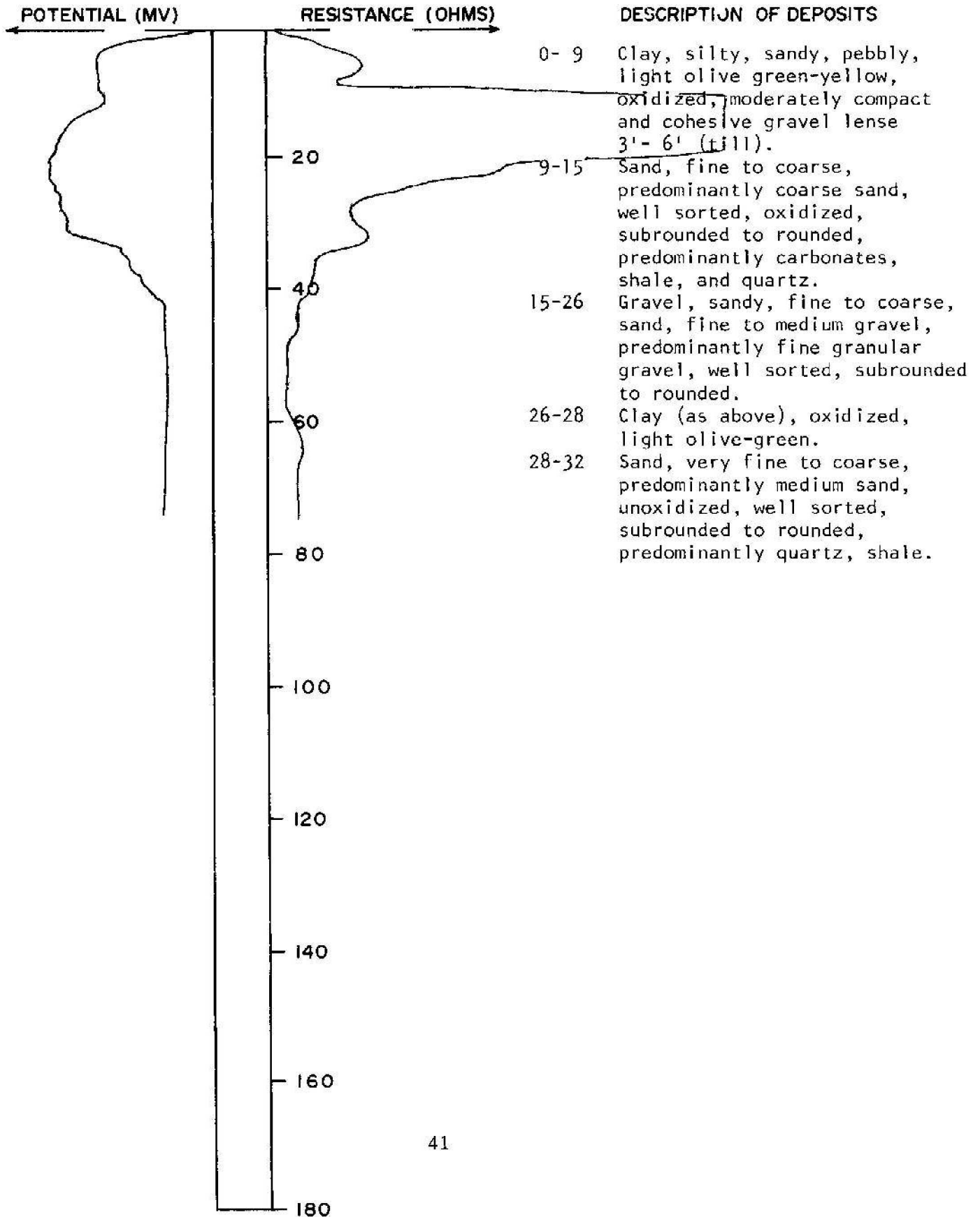


Table 3 -- Dissolved chemical constituents in water -- their effects upon usability and recommended concentration limits for domestic and municipal water supplies in North Dakota.

Constituent or Parameter	Effects of dissolved constituents on water use	Suggested limits for drinking water in North Dakota ¹	U.S. Public Health Service recommended limits for drinking water ²	Constituent or Parameter	Effects of dissolved constituents on water use	Suggested limits for drinking water in North Dakota ¹	U.S. Public Health Service recommended limits for drinking water ²
Silica (SiO ₂)	No physiological significance			Chloride (Cl)	Over 250 mg/l may impart a salty taste, greatly excessive concentrations may be physiologically harmful. Humans and animals may adapt to higher concentrations.		250 mg/l
Iron (Fe)	Concentrations over 0.1 mg/l will cause staining of fixtures. Over 0.5 mg/l may impart taste and colors to food and drink.		0.3 mg/l	Fluoride (F)	Fluoride helps prevent tooth decay within specified limits. Higher concentrations cause mottled teeth.	Limits of 0.9 mg/l to 1.5 mg/l	Recommended limits depend on average of daily temperatures. Limits range from 0.6 mg/l at 32°C. to 1.7 mg/l at 10°C.
Manganese (Mn)	Produces black staining when present in amounts exceeding 0.05 mg/l		0.05 mg/l	Nitrate (NO ₃)	Over 45 mg/l can be toxic to infants. Larger concentrations can be tolerated by adults. More than 200 mg/l may have a deleterious effect on livestock health		45 mg/l
Calcium (Ca) and Magnesium (Mg)	Calcium and magnesium are the primary causes of hardness. High concentrations may have a laxative effect on persons not accustomed to this type of water.			Boron (B)	No physiological significance. Greater than 2.0 mg/l may be detrimental to many plants		
Sodium (Na)	No physiological significance except for people on salt-free diets. Does have an effect on the irrigation usage of water.			Total dissolved solids	Persons may become accustomed to water containing 2,000 mg/l or more dissolved solids.	0-500 mg/l - low 500-1400 mg/l average 1400-2500 mg/l high over 2500 mg/l very high	500 mg/l
Potassium (K)	Small amounts of potassium are essential to plant and animal nutrition.			Hardness (as CaCO ₃)	Increases soap consumption, but can be removed by a water-softening system.	0-200 mg/l - low 200-300 mg/l average 300-450 mg/l high over 450 mg/l very high	
Bicarbonate (HCO ₃) and Carbonate (CO ₃)	No definite significance, but high bicarbonate content will impart a flat taste to water.			pH	Should be between 6.0 and 9.0 for domestic consumption		
Sulfate (SO ₄)	Combines with Calcium to form scale. More than 500 mg/l tastes bitter and may be a laxative	0-300 mg/l - low 300-700 mg/l - high over-700 mg/l - very high	250 mg/l	Specific Conductance	An electrical indication of total dissolved solids measured in micromhos per Centimeter at 25°C. Used primarily for irrigation analyses.		
Percent Sodium and Sodium Adsorption Ratio (SAR)	Indicate the sodium hazard of irrigation water.						

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