Site Suitability Review of the Dickinson Municipal Landfill

by Jeffrey Olson North Dakota State Water Commission and Phillip L. Greer North Dakota Geological Survey





Prepared by the North Dakota State Water Commission and the North Dakota Geological Survey

ND Landfill Site Investigation No. 30

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Bismarck, North Dakota 1994

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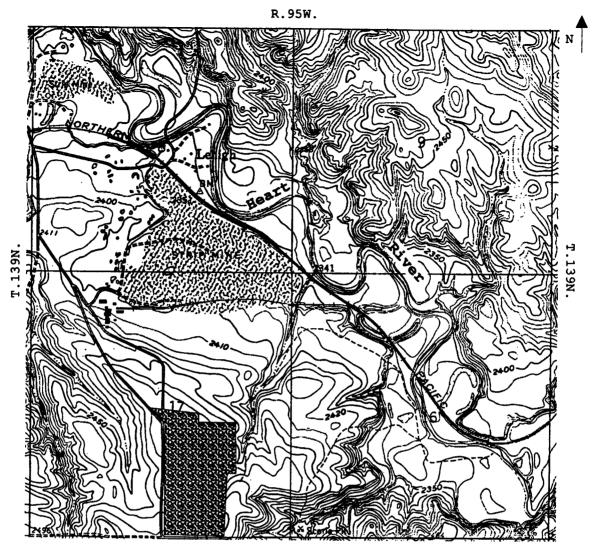
INTRODUCTION

Purpose

The North Dakota State Engineer and the North Dakota State Geologist were instructed by the 52nd State Legislative Assembly to conduct site-suitability reviews of the solid waste landfills in the state of North Dakota. These reviews are to be completed by July 1, 1995 (North Dakota Century Code 23-29-07.7). The purpose of this program is to evaluate site suitability of each landfill for disposal of solid waste based on geologic and hydrologic characteristics. Reports will be provided to the North Dakota State Department of Health and Consolidated Laboratories (NDSDHCL) for use in site improvement, site remediation, or landfill closure. A one time ground-water sampling event was performed at each site, and additional studies may be necessary to meet the requirements of the NDSDHCL for continued operation of solid waste landfills. The Dickinson municipal solid waste landfill is one of the landfills being evaluated.

Location of the Dickinson Landfill

The Dickinson municipal solid waste landfill is located five miles south of the City of Dickinson in Township 139 North, Range 95 West, SW 1/4, SE 1/4 Section 17 (Fig. 1). The landfill site encompasses approximately 45 acres of an abandoned lignite strip mine.

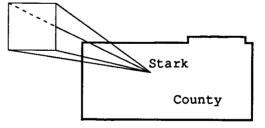


R.95W.



Landfill Boundary

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Elevation in feet above MSL (NGVD, 1929)

Figure 1. Location of the Dickinson municipal landfill in the SE 1/4 of section 17, T139N, R95W.

Previous Site Investigations

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A geotechnical and hydrogeologic report by Braun Intertec was completed on February 3, 1992 with an addendum completed on January 18, 1993. Ten monitoring wells were installed around the perimeter of the landfill and two temporary monitoring wells were installed at the base of the strip mine. Four of the monitoring wells were screened within the Lehigh lignite bed, four were screened within the mine spoils, and four were screened in the bedrock sand beneath the Lehigh lignite. Three of the four wells screened in the Lehigh lignite were dry and three of the four monitoring wells screened in the mine spoils were also dry during Braun's study.

Conclusions drawn from Braun's report were: groundwater flow is to the east toward the Heart River, there is no apparent contaminant migration from the landfill, the bottom liner meets specifications, and the thickness of the clay liner is variable.

Water quality analyses were completed for major ions, trace elements, and VOC compounds. A pH of 9.3 was detected in well MW-30 (139-095-17DAC) during this study. No anomalously large concentrations of other analytes were detected in this study.

Methods of Investigation

The Dickinson study was accomplished by means of: 1) drilling test holes; 2) constructing and developing monitoring wells; 3) collecting and analyzing water samples; and 4) measuring water levels.

Test-Drilling Procedure

The drilling method at the Dickinson landfill was based on the site's geology and depth to ground water, as determined by the preliminary evaluation. A forward-rotary drill rig was used at the Dickinson landfill because the sediments were consolidated and because the depth to the water table was expected to be greater than 70 feet. The lithologic descriptions were determined from the drill cuttings.

Monitoring Well Construction and Development

Three test holes were drilled at the Dickinson landfill, and monitoring wells were installed in all of them. Four existing monitoring wells installed by Braun Intertec were also used in this study. The number of wells installed at the Dickinson landfill was based on the geologic and topographic characteristics of the site. The depth and

intake interval of each well was selected to monitor the water level at the top of the uppermost aquifer. The wells were located around the active area of the landfill.

Wells were constructed following a standard design (Fig. 2) intended to comply with the construction regulations of the NDSDHCL and the North Dakota Board of Water Well Contractors (North Dakota Department of Health, 1986). The wells were constructed using a 2-inch diameter, SDR21, polyvinyl chloride (PVC) well casing and a PVC screen, either 5 or 10 feet long, with a slot-opening size of 0.012 or 0.013 The screen was fastened to the casing with stainless inches. steel screws (no solvent weld cement was used). After the casing and screen were installed into the drill hole, the annulus around the screen was filled with No. 10 (grain-size diameter) silica sand to a height of two feet above the top of the screen. High-solids bentonite grout and/or neat cement was placed above the silica sand to seal the annulus to approximately five feet below land surface. The remaining annulus was filled with drill cuttings. The permanent wells were secured with a protective steel casing and a locking cover protected by a two-foot-square concrete pad.

All monitoring wells were developed using a stainless steel bladder pump or a teflon bailer. Any drilling fluid and fine materials present near the well were removed to insure movement of formation water through the screen.

The Mean Sea Level (MSL) elevation was established for each well by differential leveling to Third Order accuracy.

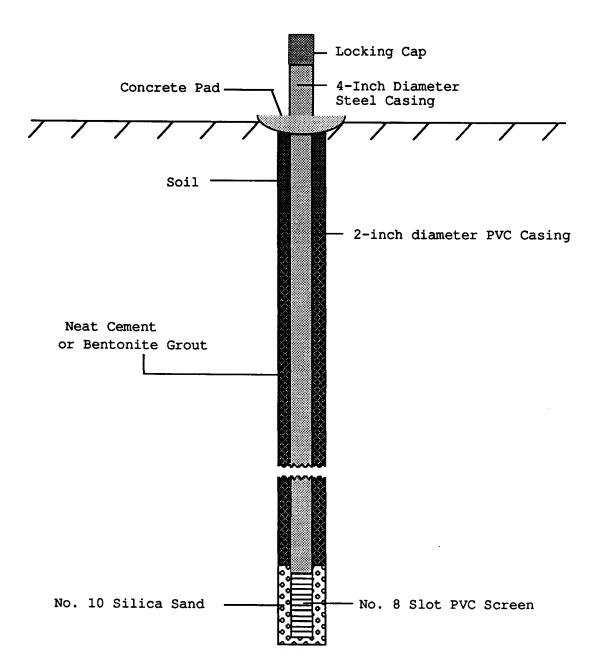
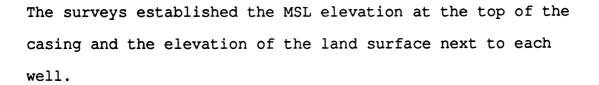


Figure 2. Construction design used for monitoring wells installed at the Dickinson landfill.



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Collecting and Analyzing Water Samples

Water-quality analyses were used to determine if leachate is migrating from the landfill into the underlying ground-water system. Selected field parameters, major ions, and trace elements were measured for each water sample. These field parameters and analytes are listed in Appendix A with their Maximum Contaminant Levels (MCL). MCLs are enforcable drinking water standards that represent the maximum permissible level of a contaminant as stipulated by the U.S. Environmental Protection Agency (EPA).

Water samples were collected using a bladder pump constructed of stainless steel with a teflon bladder. A teflon bailer was used in monitoring wells with limited transmitting capacity. Before sample collection, three to four well volumes were extracted to insure that unadulterated formation water was sampled. Four samples from each well were collected in high-density polyethylene plastic bottles as follows:

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1) Raw (500 ml)
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- 2) Filtered (500 ml)
- 3) Filtered and acidified (500 ml)
- 4) Filtered and double acidified (500 ml)

The following parameters were determined for each sample. Specific conductance, field pH, bicarbonate, and carbonate were analyzed using the raw sample. Sulfate, chloride, nitrate*, and dissolved solids were analyzed using the filtered sample. Calcium, magnesium, sodium, potassium, iron, and manganese were analyzed from the filtered, acidified sample. Cadmium, lead, arsenic, and mercury were analyzed using the filtered double-acidified samples.

One well was sampled for Volatile Organic Compounds (VOC) analysis. This sample was collected at a different time than the standard water-quality sample. The procedure used for collecting the VOC sample is described in Appendix B. Each sample was collected with a plastic throw-away bailer and kept chilled. These samples were analyzed within the permitted 14-day holding period. The standard waterquality analyses were performed at the North Dakota State Water Commission (NDSWC) Laboratory and VOC analyses were performed by the NDSDHCL.

Water-Level Measurements

Water-level measurements were taken at least three times at about two-week intervals. The measurements were taken using a chalked-steel tape or an electronic (Solnist 10078) water-level indicator. These measurements were used to determine the shape and configuration of the water table.

^{*} No special preservative techniques were applied to nitrate samples and as a result reported nitrate concentrations may be lower than actual.

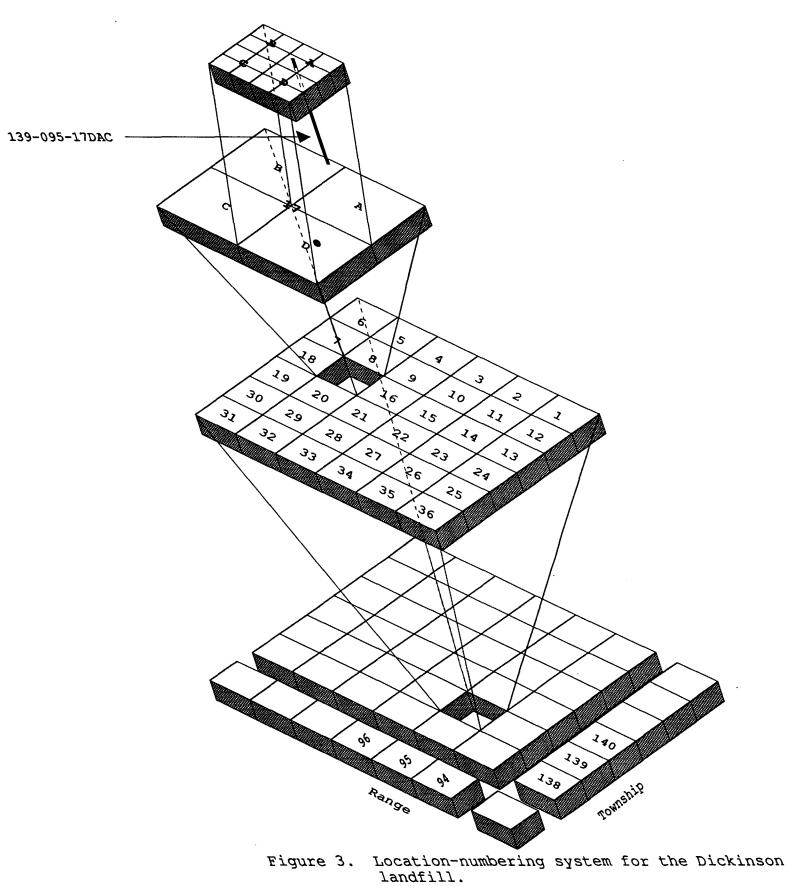
Location-Numbering System

The system for denoting the location of a test hole or observation well is based on the federal system of rectangular surveys of public land. The first and second numbers indicate Township north and Range west of the 5th Principle Meridian and baseline (Fig. 3). The third number indicates the section. The letters A, B, C, and D designate, respectively, the northeast, northwest, southwest, and southeast quarter section (160-acre tract), quarter-quarter section (40-acre tract), and quarter-quarter-quarter section (10-acre tract). Therefore, a well denoted by 139-095-17DAC would be located in the SW1/4, NE1/4, SE1/4, Section 17, Township 139 North, Range 95 West. Consecutive numbers are added following the three letters if more than one well is located in a 10-acre tract, e.g. 139-095-17DAC1 and 139-095-17DAC2.

GEOLOGY

Regional Geology

The Dickinson landfill is located in the former Husky Mine pit in section 17, T139N, R95W. The mine is south of the Heart River in an area of dissected bedrock. Several ravines drain toward the Heart River from the area surrounding the mine. Two ravines east of the site are



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eroding toward the mine (Fig. 4). The valley of the Heart River, located about three-fourths mile from the mine, contains alluvium, consisting of clay, silt, sand, and gravel.

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Two lignite beds, the Dickinson and Lehigh, were mined at the site. These beds are part of the Sentinel Butte Formation, which also includes clay, silt, sand, sandstone, and limestone. The Sentinel Butte Formation is underlain by the Bullion Creek, Slope, Cannonball, Ludlow, Hell Creek, and Fox Hills Formations.

Schmid (1980) identified a north-south trending anticline by mapping the elevation of the Lehigh bed. The axis of the anticline is near the west side of the mine pit. The east limb dips about 150 feet per mile (1.6 degrees), while the west limb dips less than 1 degree. Schmid also observed a fault with a displacement of about 3 feet in the southeast corner of the pit. Additional faults may be present near the mine, but faults with minor displacement are difficult to define with subsurface data.

Local Geology

The mine pit is more than 100 feet deep. The walls of the pit consist of clay with interbedded sand and lignite. The Dickinson lignite is about 4 to 8 feet thick, and the Lehigh lignite is about 7 to 17 feet thick (Fig. 5). The mine operator spread and packed spoil material on the bottom

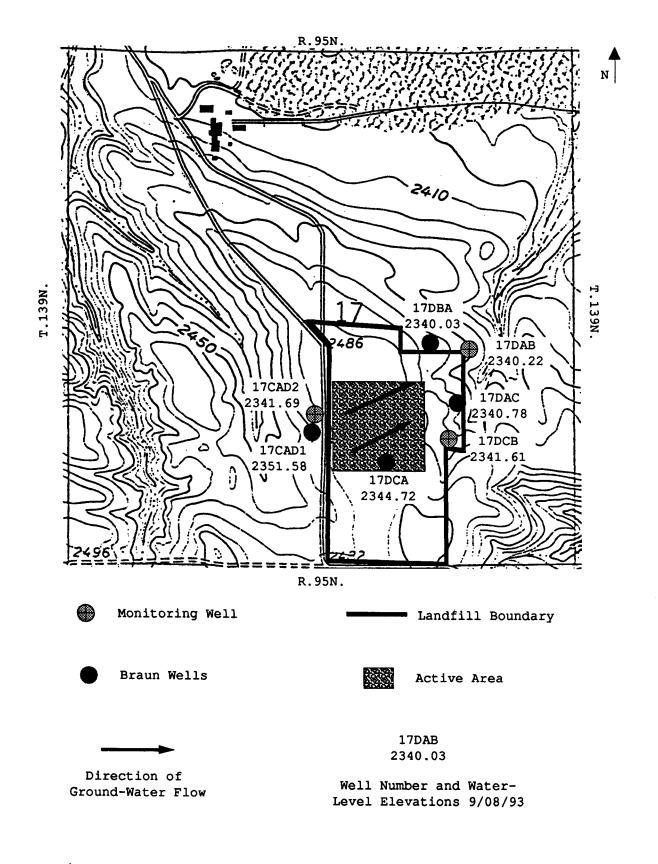
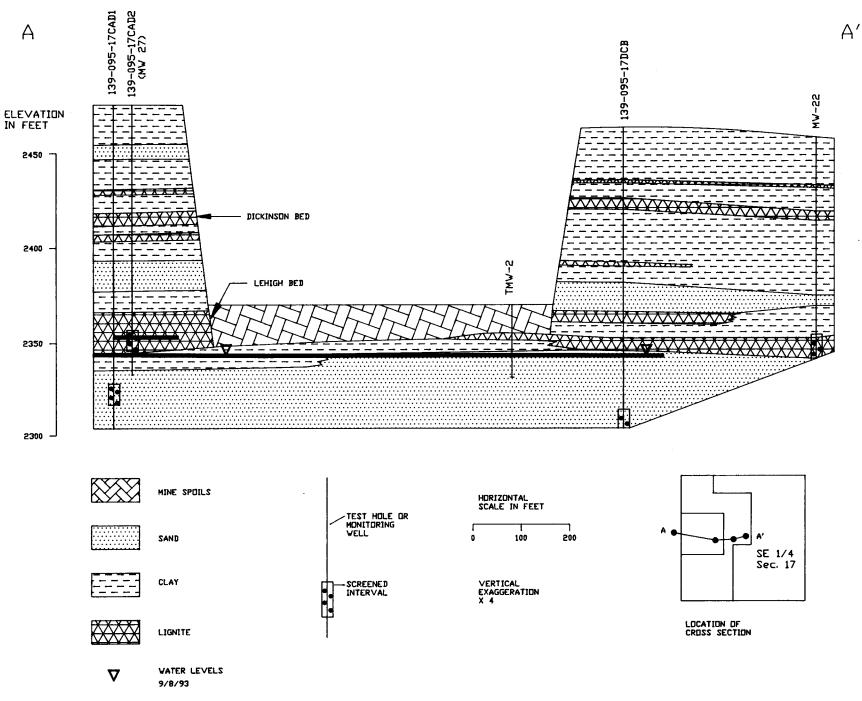


Figure 4. Location of monitoring wells at the Dickinson municipal landfill.



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Figure 5. Geohydrologic section A-A' in the Dickinson landfill.

of the pit to serve as a liner. Soil borings drilled within the pit (Braun, 1992, 1993) indicate that the thickness of the spoil material varies from 1.5 feet to 15 feet.

The compacted spoils are underlain by a thin layer of clay that ranges from 3 feet in Braun SB-10 to 15 feet in Braun TMW-1. The clay is underlain by a thick layer of finegrained to medium-grained, silty sand. The sand is at least 45 feet thick as indicated by test hole 139-095-17DCB (Fig. 5, lithologic logs in Appendix C). None of the test holes at the mine drilled through the sand layer.

Clinker beds are exposed in the ravines to the east and west of the mine. These beds are stratigraphically higher than the Lehigh bed, and likely represent outcrops of the Dickinson lignite bed.

The Lehigh lignite bed is exposed at the surface north of the Husky Mine in the Heart River valley. The Lehigh bed was mined along the Heart River in the Lehigh, Binek, and Pittsburgh mines in sections 7 and 8, T139N, R95W. Because of the structural dip the Lehigh bed is not exposed along the river to the east of the mine. Structure contours for this area (about the middle of section 16) indicate that the Lehigh bed is about 100 feet below the Heart River (Schmid, 1980).

HYDROLOGY

Surface-Water Hydrology

The Heart River is located about three-quarters of a mile north and east of the landfill (Fig. 1). The Heart River valley is the local drainage basin for the area surrounding the landfill. Ravines located on the east and the west sides of the landfill drain surface-water runoff toward the Heart River. The Heart River should not be affected by surface runoff from the landfill due to its distance from the landfill and the depth of the disposal pit.

A few stock dams are located within a two-mile radius of the landfill. These stock dams should not be affected by contaminant migration from the landfill due to their upgradient location.

Regional Ground-Water Hydrology

The Dickinson landfill is located in an area of unglaciated topography and only bedrock aquifers exist beneath the landfill site. The uppermost aquifer is located in the Sentinel Butte Formation and occurs in undifferentiated lignite beds and in the fine to mediumgrained sand layers throughout the formation. The Sentinel Butte aquifer is the main source of domestic water supply for the area. Locally, sand and fractured lignite layers beneath

the landfill may be susceptible to contaminant migration from the landfill.

The Bullion Creek aquifer underlies the Sentinel Butte aquifer in the area of the landfill. This aquifer is located at a depth of about 550 feet. The Bullion Creek aquifer is generally characterized by a sodium-bicarbonate type water. This aquifer should not be affected by contaminant migration from the landfill due its depth and the occurrence of intervening clay layers.

The Hell Creek aquifer underlies the Ludlow Formation and occurs at a depth of about 800 feet (Trapp, et al., 1975). The Hell Creek Formation overlies the Fox Hills aquifer, which is located at a depth of about 1,020 feet (Trapp, et al., 1975) These aquifers should not be affected by contaminant migration from the landfill due to their depth and the occurrence of intervening clay layers.

Local Ground-Water Hydrology

Three monitoring wells were installed to monitor the layer of bedrock sand of the Sentinel Butte Formation that underlies the Lehigh lignite layer. Four existing monitoring wells from Braun (1991) were also used to determine the occurrence and movement of ground water in this sand aquifer.

The Lehigh and Dakota lignite beds were penetrated during the drilling process. These lignite beds were dry during the time of drilling. A clay aquitard about 10 feet

thick occurs between the Lehigh lignite and the underlying sand aquifer.

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Four water-level measurements were taken over about a seven-week period (Appendix E). Monitoring well 17CAD1 is completed in the Lehigh lignite and monitoring well 17CAD2 is completed in the underlying sand aquifer in the Sentinel Butte Formation (Fig. 4). Water-level measurements indicate downward ground-water flow from the Lehigh lignite to the Sentinel Butte sand (Fig. 5). The volume of downward flow probably is small due to the low intervening hydraulic conductivity clay layer. The direction of local ground-water flow is to the east toward the Heart River valley (Fig. 4).

Water Quality

Chemical analyses of water samples are shown in Appendix F. An anomalously high pH value of 9.97 was detected in well 17DBA. An elevated pH at this well was also detected by Braun (1993). The source of the high pH was not determined in this study. The water in the Sentinel Butte sand aquifer is characterized by a sodium-bicarbonate type water. Anomalously large concentrations of other analytes, including trace elements, were not detected in this study.

The results of the VOC analysis, from well 17DAB, are shown in Appendix G. The analysis detected the compounds tetrahydrofuran at a concentration of 140 μ g/L and 2-Butanone (MEK) at a concentration of 228 μ g/L. These compounds are

man-made compounds used in glues and liquid cements for fabricating packages and polyvinyl-chloride materials. The source of these compounds may to be due to well construction. A later sampling event by Braun Intertec on January 12, 1994, indicated a reduced tetrahydrofuran concentration (24 μ g/L) and no detection of MEK. Periodic monitoring at this well may be appropriate to evaluate temporal fluctuations of these two compounds.

CONCLUSIONS

The Dickinson landfill is located in the former Husky Mine Pit. The Dickinson and Lehigh lignite beds were mined at this location. The landfill is situated within the Sentinel Butte Formation which also includes zones of sand, sandstone, silt, clay, and limestone. A previous investigation at the site indicates the bedrock forms a north-south trending anticline. The axis of the anticline is along the west side of the landfill. A fault observed in the pit had a displacement of about 3 feet.

The base of the pit was covered with spoil material ranging in thickness from 1.5 to 15 feet. The spoil material was used as the liner for the refuse cell. The spoil material is underlain by a layer of clay ranging in thickness from 3 feet to 15 feet. This layer of clay is underlain by a layer of fine to medium-grained silty sand that is at least

45 feet thick and appears to dip to the east towards the Heart River valley.

The Heart River is located about three-quarters of a mile north and east of the landfill and the Heart River watershed includes the area around the landfill. The Heart River should not be susceptible to contaminant migration from the landfill.

The uppermost aquifer in the study area occurs within the Sentinel Butte Formation. This aquifer occurs in undifferentiated lignite beds and in fine to medium-grained sand layers. This aquifer is the main source of domestic water supply for the area.

At the time of this study the Dickinson and Lehigh lignite beds appeared to be dry with the uppermost aquifer occurring in the fine to medium-grained sand beneath the lignite. Water-level measurements indicate downward groundwater flow from the Lehigh lignite to the Sentinel Butte sand. The volume of downward flow probably is small due to the low intervening hydraulic conductivity clay layer. The direction of local ground-water flow is to the east toward the Heart River valley. The Sentinel Butte sand aquifer may be susceptible to contaminant migration beneath the landfill due to the varying thickness of the overlying clay aquitard.

Chemical analyses indicated an anomalously high pH in well 17DBA. The high pH at this well was also detected in previous investigations. The source of this pH was not determined. Anomalously large concentrations of other

analytes, including trace elements, were not detected in this study. Therefore, contaminant migration from the landfill was not indicated.

The VOC analysis from well 17DAB detected the compounds tetrahydrofuran and 2-Butanone. The source of these compounds may to be due to well construction. Periodic monitoring at this well may be appropriate to evaluate temporal fluctuations of these compounds.

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APPENDIX A

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WATER QUALITY STANDARDS AND CONTAMINANT LEVELS

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Water Quality Standards and Contaminant Levels

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appearance	color/odor
PH	6-9(optimum)
specific conductance	
temperature	

Constituent	MCL (Ug/L)
Arsenic	50
Cadmium	10
Lead	50
Molybdenum	100
Mercury	2
Selenium	10
Strontium	*

*EPA has not set an MCL for strontium. The median concentration for most U.S. water supplies is 100 $\mu g/L$ (Hem, 1989).

	SMCL (mg/L)
Chloride	250
Iron	>0.3
Nitrate	50
Sodium	20-170
Sulfate	300-1000
Total Dissolved Solids	>1000

Recommended Concentration Limits (mg/L)

Bicarbonate	150-200
Calcium	25-50
Carbonate	150-200
Magnesium Hardness	25-50 >121 (hard to very hard)

APPENDIX B

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SAMPLING PROCEDURE FOR VOLATILE ORGANIC COMPOUNDS

SAMPLING PROCEDURE FOR 40ML AMBER BOTTLES

Sample Collection for Volatile Organic Compounds

by

North Dakota Department of Health and Consolidated Laboratories

- 1. Three samples must be collected in the 40ml bottles that are provided by the lab. One is the sample and the others are duplicates.
- 2. A blank will be sent along. Do Not open this blank and turn it in with the other three samples.
- 3. Adjust the flow so that no air bubbles pass through the sample as the bottle is being filled. No air should be trapped in the sample when the bottle is sealed. Make sure that you do not wash the ascorbic acid out of the bottle when taking the sample.
- 4. The meniscus of the water is the curved upper surface of the liquid. The meniscus should be convex (as shown) so that when the cover to the bottle is put on, no air bubbles will be allowed in the sample.

convex meniscus

- 5. Add the small vial of concentrated HCL to the bottle.
- 6. Screw the cover on with the white Teflon side down. Shake vigorously, turn the bottle upside down, and tap gently to check if air bubbles are in the sample.
- 7. If air bubbles are present, take the cover off the bottle and add more water. Continue this process until there are no air bubbles in the sample.
- 8. The sample must be iced after collection and delivered to the laboratory as soon as possible.
- 9. The 40 ml bottles contain ascorbic acid as a preservative and care must be taken not to wash it out of the bottles. The concentrated acid must be added after collection as an additional preservative.

APPENDIX C

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LITHOLOGIC LOGS OF WELLS AND TEST HOLES

139-095-17CAD2						
Date Completed:8/4/93L.S. Elevation (ft):2485.01Depth Drilled (ft):180Screened Interval (ft):158-168		NDSWC Purpose: Well Type: Aquifer: Source:	Observation Well 2" PVC UND			
		:	Owner: Lithologic Log	DICKINSON LANDFILL		
Unit	Descript	ion		Depth (ft)		
TOPSOIL	SANDY			0-2		
CLAY	STIFF, OXI	DIZED, BEDR	OCK, OLIVE	2-15		
CLAY	MOTTLED, F	EDDISH -BRO	WN, SILTY	15-16		
CLAY	OXIDIZED,	OLIVE		16–18		
CLAY	MEDIUM GRA	Y		18-20		
CLAY	OLIVE			20-29		
LIGNITE				29-30		
SAND	SILTY, YEI	LOWISH-BROWI	N	30–37		
CLAY	OLIVE			37–57		
LIGNITE				57–59		
CLAY	MEDIUM GRA	Y		59-68		
LIGNITE	DAKOTA BEE	1		68-74		
CLAY	LIGHT GREE	N		74-80		

LIGNITE

.

CLAY	DARK GRAY	82-90
CLAY	LIGHT GREEN	90-92
SAND	LIGHT GREEN, VERY FINE GRAIN	92-108
CLAY	SILTY, LIGHT GRAY	108-116
SANDSTONE		116-117
CLAY	LIGHT GRAY	117–122
LIGNITE	LEHIGH BED	122-142
67 N Y		140 150
CLAY	GRAYISH-GREEN	142-150
SAND	FINE GRAIN, LIGHT GREEN	150-152
SAND	MEDIUM GRAIN, GREEN	152-180

80-82

Date Completed L.S. Elevation Depth Drilled Screened Inter	(ft): (ft):	8/5/93 2440.22 140 122-132		95-17DAB DSWC Purpose: Well Type: Aquifer: Source: Owner:	Observation Well 2" PVC UND DICKINSON LANDFILL
			Lithol	logic Log	
Unit	Descript	ion			Depth (ft)
TOPSOIL					0-1
CLAY	SPOILS, ME	DIUM GRAY,	STIFF		1-14
LIGNITE					14-19
CLAY	MEDIUM GRA	Y, SPOILS			19-92
SAND	VERY FINE	GRAIN, SIL	TY, LIG	HT GRAY	92-113
SANDSTONE	HARD, FINE	GRAIN			113-114
CLAY					114-124
SAND	MEDIUM GRA	IN			124-140

		-	139-095				
Date Completed L.S. Elevation Depth Drilled Screened Inter	(ft): (ft):	8/5/93 2463.51 160 150-160	N 1 1	Purpo se: Well Type: Aquifer: Source:		Observation 1 2" PVC UND	
				Owner:		DICKINSON LA	NDE LL
			Litholog	gic Log			
Unit	Descript	ion					Depth (ft)
TOPSOIL							0-1
CLAY	SILTY, LIC GRAY CLAY		SH-ORANG	E, INTERMIXE	d med:	IUM	1-26
CLAY	MEDIUM GRA	AY					26-28
LIGNITE							28-29
CLAY	MEDIUM GRA	AY, STIFF					29-35
CLAY	BROWNISH-(OF LIGNITH		THIN TWO	TO THREE IN	CH LAY	YER	35-38
LIGNITE							38-43
CLAY	SILTY, MEI	DIUM GRAY					43-46
CLAY	LIGHT GRE	EN, VERY FIN	NE SAND				46-55
CLAY	GRAYISH-B	ROWN, LIGNI	TE CHIPS				55-72
LIGNITE	LIGNITE L	AYER APPROX	. SIX IN	CHES THICK			72-72.6
CLAY	GRAYISH-B	ROWN, LIGNI	TE CHIPS				72.6-82

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SAND	FINE GRAIN, CLAYEY	82-98
LIGNITE	DAKOTA BED	98-102
CLAY		102-112
LIGNITE		112-115
SAND	FINE GRAIN, TRACE OF SILT	115–152
SANDSTONE	INDURATED	152–157
SAND	MEDIUM GRAIN	157-160

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APPENDIX D .

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LITHOLOGIC LOGS OF WELLS AND TEST HOLES FROM PREVIOUS STUDIES.

BRAUN

INTERTEC

	PROJE	CT: CI	FEX-9	1-00	7L	BORING	:		SB-10
		Cl	TY O	F D	OLOGIC ASSESSMENT ICKINSON SANITARY LANDFILL N, NORTH DAKOTA	LOCATI See F	ON: igure £	5.	
						DATE:	8/30	/91	SCALE: 1" = 10'
(.180	Elev. 2365.6	Depth 0.0	AST Symł		Description of Materials (ASTM D 2488)		BPF	WL	Tests or Notes
tive termino	2352.6	13.0 13.0	SM		SPOILS Consists mainly of clay, silt, and fingrained sand. The proportion, thickness, and depth of each constituent varies. SILTY SAND very fine grained, dark greenish gray (5GY4/1), dense, damp.				Sample #194(1-1.5) #195(7-7.5) #196(12-12.5)
tion	2342.6	23.0-							#197(20-20.5)
lua	- 23 39.6	26. 0 -	CL		<u>CLAY</u> with silt, greenish gray (5GY6/1) little very fine grained sand, rather stiff, moist.)			TWT-3(23-24.5)
eva	2 337.6	28.0	SM		SILTY SAND fine to medium grained, dark				#198(25-25.5) Water level at 25.5'
tes for (-		SC		greenish gray (5GY4/1), poorly graded, loose to medium dense, moist. <u>CLAYEY SAND little silt, dark greenish gray</u> (5GY4/1), moist.				(2340.1' elev.) #199(29.5-30)
Standard Pla		1111			wet to waterbearing				#200(35.5-36)
and	-	50.0							#201(42-42.5) #202(43.5-44)
(See Repor	2315.6			<i>22</i>	END OF BORING.				

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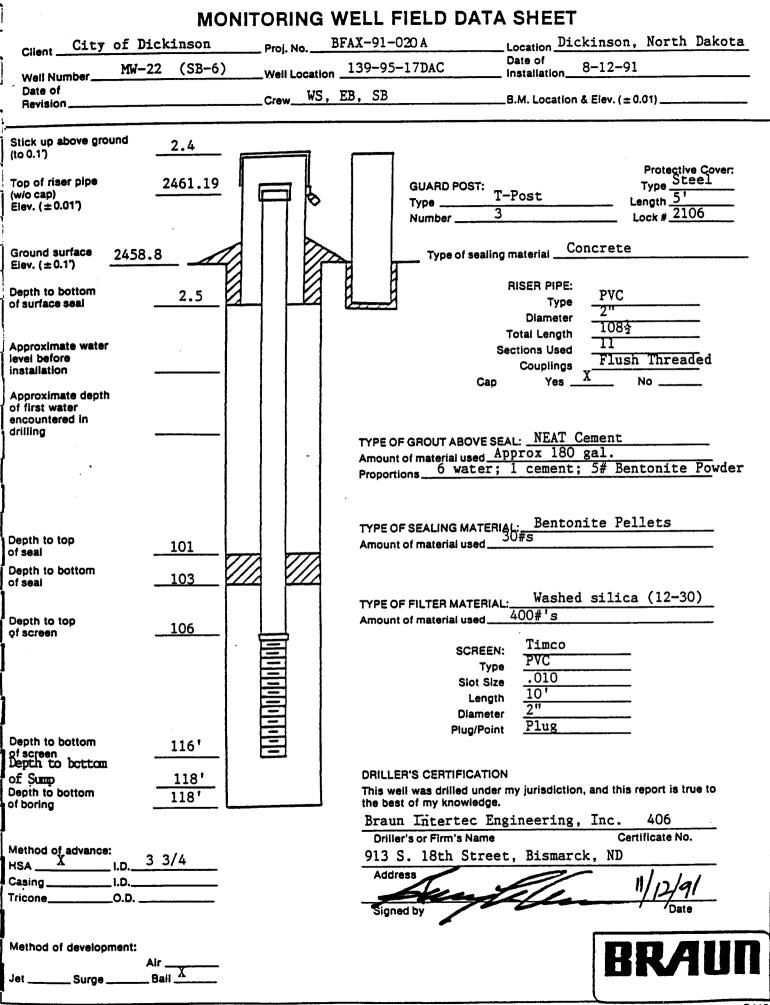
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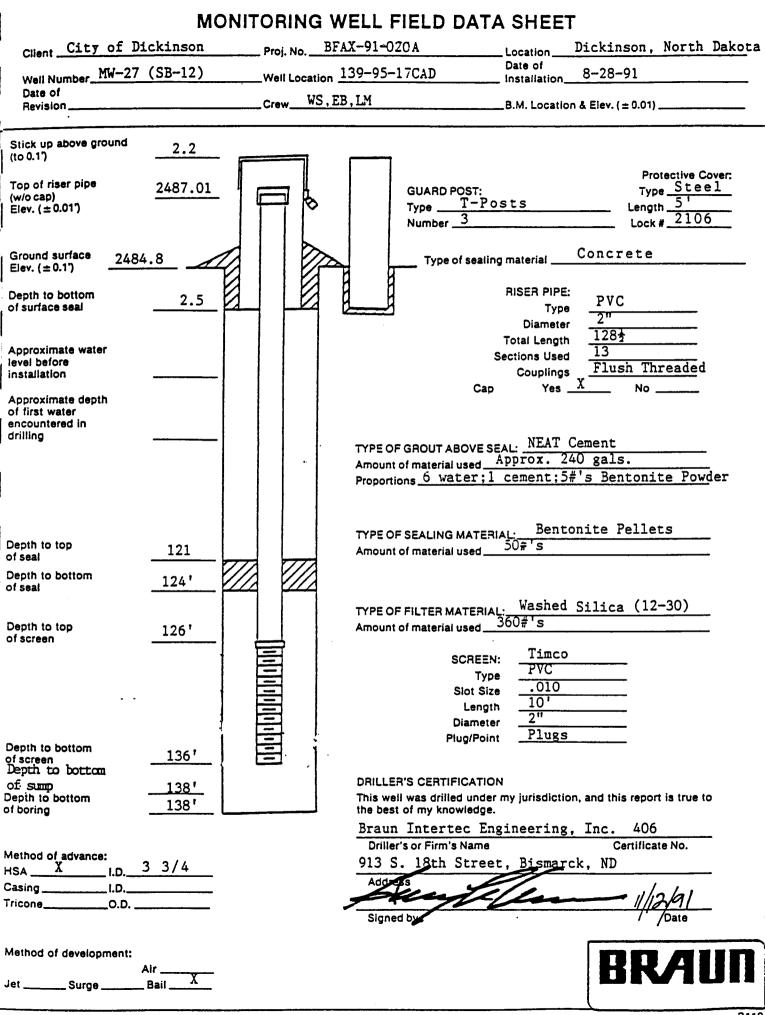
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PROJE	CT: C	FEX-9	1-00	7L ·	BORING	:		SB-6	(cont.)
	C	TY O	F DI	DLOGIC ASSESSMENT CKINSON SANITARY LANDFILL I, NORTH DAKOTA	LOCATI MW-		9-95-	17DAC	
					DATE:	8/9	/91	SCALE:	$1^{*} = 10^{\circ}$
Elev.	Depth	ASTI Symb		Description of Materials (ASTM D 2488)		BPF	WL.	Tests or	Notes
Elev.				SILT light gray (2.5YN6/).				#48(80-80.5)	
23 72.8 2 369.8	86. 0 89.0	SM		<u>SILTY SAND very fine to fine grained, light</u> gray (2.5YN6/), some bedding apparent.	;			#49(86.5-87)	
 2365.3		CL		CLAY somewhat cemented.				#50(91-91.5)	
	 98.0-	ML		<u>SILT</u> with very fine-grained sand, light gray (2.5YN6/). organic laminae from 97' to 98'				#51(96-96.5)	
-	1 1 1	CL		CLAY dark gray (5Y4/1), with laminae of si and fine sand, damp.	lt			#52(101-101.	5)
2 352.8	106. 0			LIGNITE black with iron-stained surfaces,	<u> </u>			#53(107-107.	ຽ
				dry, LEHIGH LIGNITE.				#54(110-110.	-
- 23 42.8 2 340.8	 116. 0 118.0	СН		CLAY dark gray (5Y4/1), with minor lenses					-
				of interbedded sand.	/			#55(116.5-11	/)
				END OF BORING. Monitoring well MW-22 installed and					
				screened from 106' to 116'.					
-									
-									
-									
-	-								



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				L	NT	ERTEC				
PROJECT: 0	CFEX-91-0	07L	BORING: SB-6							
(CITY OF D	OLOGIC ASSESSMENT ICKINSON SANITARY LANDFILL N, NORTH DAKOTA	LOCATI MW-		-95-:	17DAC				
			DATE:	8/9/	91	SCALE:	1" = 10			
Elev. Depth 2458.8 0.0	ASTM Symbol	Description of Materials (ASTM D 2488)		BPF	WL	Tests or	Notes			
	CL.	<u>CLAY</u> with some interbedded silt, olive (5Y5/4), organic films common on bedding surfaces, dry, no HCl reaction on white crystallizations. more clay and less silt, olive brown (2.5Y4/3 white crystallizations exhibit moderate reaction to HCl, damp.)			Sample #32(1 #33(6-6.5)	.5-2)			
					-	#34(16-16.5) #35(21-21.5)				
- 2432.3 26.3 2430.8 28.0 		grades to a very dark gray (5Y3/1) LIGNITE with carbonaceous clay, black, wet CLAY dark gray (2.5YN4/), minor silt, dam				#36(26.5-28)	(composite)			
- -		2-inch thick carbonaceous clay at 34'				#37(32-32.5)				
2420.8 38.0 		LIGNITE black, fissile, dry, DICKINSON LIGNITE.				#38(36-36.5) #39(38-41.5)	(composite)			
2415.3 43.4 		<u>CLAY</u> gray (10YR5/1), little silt, trace of very fine sand along bedding surfaces.	/			#40(44.5-45)				
2412.8 46.4 2411.3 47.5	SP	CLAY geenish gray (5GY5/1), damp. SAND very fine-grained, greenish gray	/			#41(46.5-47)				
2408.3 50.4	CL	(5GY5/1), damp to moist. CLAY greenish gray (5GY5/1), damp.]			#42(49-49.5)				
		CLAY very dark gray (5Y3/1), interbedded with abundant .5 to 1 inch thick carbonaceous	/ \$			#43a(52.5-53))			
- - -		layers, trace of pyrite within these layers.				#43b(56-56.5)			
2394.3 64.5		carbonaceous clay from 61' to 64.5'				#44(60-60.5)				
2390.8 68.0		<u>CLAY</u> dark greenish gray (5GY4/1), very dense.	·			#45(65.5-66)				
2388.3 70.4		<u>CLAY</u> gray to dark gray (2.5YN5/ to N6/). transition from clay to very fine sand from				#46(69-69.5)				
		70' to 71' SANDY CLAY very fine-grained with silt,]			#47(72-72.5)				
2381.8 77.0		light gray (2.5YN6/), minor laminae of clay. interbedded with clay of same color,	Г							



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DDOIE	<u>ст. с</u>	FFV 4	1 00	71	BORING: SB-12							
PROJE	\mathbf{C} : \mathbf{C}	FEX-9	71-00									
	C	ITY C)F D	OLOGIC ASSESSMENT ICKINSON SANITARY LANDFILL N, NORTH DAKOTA	LOCATI MW-)-95-	17CAD				
					DATE:	8/20	/91	SCAL	E:	1" = 10		
Elev. 2484.8	Depth 0.0	AST Sym1		Description of Materials (ASTM D 2488)		BPF	WL	Tests	or	Notes		
2483.8		ML	ПП	<u>SILT</u> brown (10YR4/3), some clay, roots.		<u> </u>	+					
-	-	CL		SILTY CLAY light yellowish brown	/							
-				(2.5Y6/4), calcareous, roots present, mottled	l .			Sample #1	-	5-3)		
			Ø					#120(7-7.5)			
- - 		-						#121(11.5-	12)			
-	- 17.0	СН		CLAY little silt, light olive gray (5Y5/3), dr	у			#122(16-16	5.5)			
				vertical fractures evident, iron and manganes stained, damp	e			#123(19.5-	20)			
-				very stiff and dense clay, olive (2.5Y5/4)				#124(26.5-	27)			
2452.8	32.0-	SM		1" soft lignite layer at 30.5' SILTY SAND fine grained, light gray				#125(32-32	2.5)			
2 449.8 -	35.0-	CL		(5Y6/1). CLAY with silt, olive brown (2.5Y5/3),				#126(35-35	5.5)			
2446.3	38.5		\mathbb{M}	dense, trace of sand.	_							
2444.3	40.5	ML CL		CLAYEY SILT with trace of fine grained sand, light gray and dark brown alternating laminae.	 [#127(38.5-	39)			
-	111			CLAY olive brown (2.5Y5/3), oxidized fractures present.]			#128(45.5-	46)			
				gypsum crystals present				#129(49-49	9.5)			
2428.8 2427.8	56. 0 57.0	CL						#130(54.5-	55)			
-	11 111	CL		<u>CLAY</u> carbonaceous, dark gray (7.5YR4/0), very stiff, damp. trace of lignite fragments				#131(60. 5 -	61)			
2417.8	67.0-			LIGNITE DICKINSON LIGNITE				#132(66.5 ⊣	67)			
241 3.8	7 1.0	CL		CLAY with little silt, dark gray (10YR6/1).				#133(72-72	.5)			
-								#134(75-75	-			
- 	- 			BRAUN - 11/14/91				·	SB-12	page 1 of		

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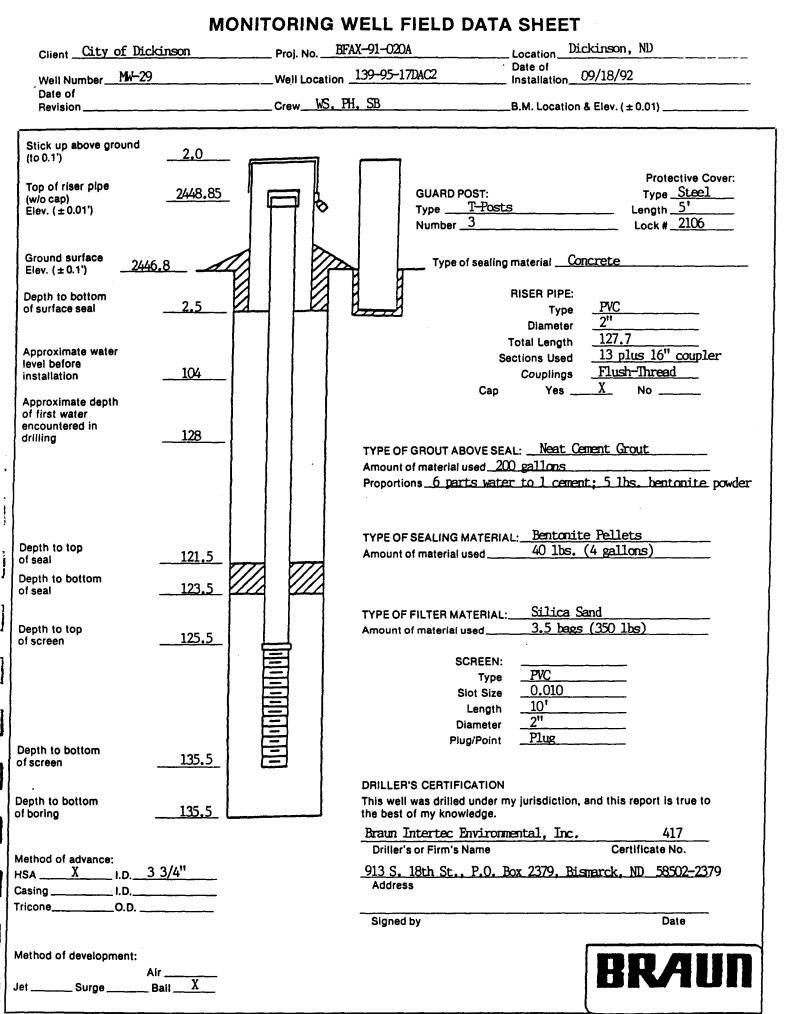
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	CT: C	FEX-9	1-00	97L	BORING: SB-12 (cont.)						
	C	ITY O	FD	OLOGIC ASSESSMENT ICKINSON SANITARY LANDFILL N, NORTH DAKOTA	LOCATI MW-	ION: 27: 13	9-95-	17CAD			
					DATE:	8/20)/91	SCA	LE:	1" = 10'	
Elev.	Depth	AST Symb		Description of Materials (ASTM D 2488)		BPF	WL	Tests	or	Notes	
2396.8	88.0- 	Symt		(ASTM D 2488) 4" lignite layer at 84' <u>SILTY SAND fine grained</u> , light gray (2.5Y6/0), dry. <u>CLAY and SILT alternating deposits of</u> clay-rich and silt-rich sediments, some layers contain small amounts of fine grained sand, colors range between light and dark gray. <u>SILTY SAND fine grained sand, light gray</u> (5Y6/1), some silt, trace of clay, some				#135(82- #136(84.: #137(91.: #138(96-9 #139(101 #140(104 #141(107 #142(111) #143(117 #144(119) #145(125 #146(127) #145(125 #146(127) #148(132) #149(139)	5-85) 5-92) -101.5 -104.5 .5-108 -111.5 -117.5 -117.5 -119.5 .5-126 -127.5 5-130 5-133)))))	



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LOG OF BORING

	PROJ	ECT: B	FAX-91-	020A	BORING	G:	М	W-29	- <u></u>			
		C	ITY OF I	EOLOGIC ASSESSMENT DICKINSON SANITARY LANDFILL N, NORTH DAKOTA	LOCAT 139-9	TON: 95-17	DAC2	2	SCALE: 1" = 10'			
					DATE:	9/1	7/92	SCAL	.E:	1" = 10'		
(.090	Elev. 2446.8	Depth 0.0	ASTM Symbol	Description of Materials (ASTM D 2488)		BPF	WL	Tests	or	Notes		
TITITITITITITITITICS (See Report and Standard Plates for evaluation and descriptive termi		22		SPOILS consists mainly of clay, silt, and grained sand, with proportions, thicknudepth of each constituent variable.	ess, and				-29	page 1 of 2		

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	PROJE	CT: BI	FAX-91-	020A	BORING: MW-29 (cont.)						ont.)	
		Cl	ITY OF I	OLOGIC ASSESSMENT DICKINSON SANITARY LANDFILL N, NORTH DAKOTA	LO	CAT 139-	ION: 95-17)	DAC	2			
					DA	TE:	9/17	/92	SCA	LE:	1	" = 10'
(,180	Elev.	Depth	ASTM Symbol	Description of Materials (ASTM D 2488)			BPF		Tests		or	Notes
ber transf		128.0	CL SP	CLAY with silt, dark gray (5Y 4/1), fine sand, moist. POORLY GRADED SAND medium greenish gray (5GY 5/1), waterbearin END OF BORING END OF BORING	grain			₽		BG: -110 -115 -120 -125 -130 -135	S) 5) 5) 5) 5 T 5 T 5) 5)	2341.01 ALLED O 135.5

		MONI	TORI		ELL FIEL	D DATA	SHEET			
	Client City of Dickir	son	Proj. N	o. <u> </u>	-91-020A		Location <u>Dic</u>	cinson,	ND	
	Well NumberMW-30		Well Lo	ocation	139-95-17DBA		Date of Installation_0	9/22/92		
	Date of Revision						B.M. Location 8	Elev. (± (0.01)	
	Stick up above ground (to 0.1')	2.48								
	Top of riser pipe (w/o cap) – Elev. (±0.01')	2455.88	F	Ø	Тур	ARD POST: <u>T-Posts</u> hber <u>3</u>			Protective Type <u>Stee</u> ength <u>5'</u> Lock # <u>210</u>	<u>el</u>
	Ground surface 2453.4 Elev. (± 0.1 ')					Type of sealing	material <u>Cor</u>	ncrete	<u> </u>	
	Depth to bottom of surface seal	_2.5	┥┝				RISER PIPE: Type Diameter			
	Approximate water level before installation	113					Total Length sections Used Couplings		us 16" cou -Thread	-
	Approximate depth of first water encountered in drilling	122				Cap DUT ABOVE Sf aterial used	Yes	ment	No	_
	Depth to top of seal Depth to bottom	<u>118.9</u> 120.9			TYPE OF SE	<u>6 parts wat</u> ALING MATER aterial used	10.51	nt: 511 te Pelle (4 galle	ets	te powder
	of seal Depth to top of screen	122.9				TER MATERIA		Sand 2s (350	lbs)	
			1010101010101010			SCREEN Typ Slot Siz Lengt Diamete	PVC 0.010 h 10'		 	
	Depth to bottom of screen	127.9				Plug/Poir	nt <u>Plug</u>		_	
j	Depth to bottom 1 of boring				This well w	CERTIFICATION as drilled under my knowledge	r my jurisdictio	on, and thi	is report is tr	ue to
	Method of advance: HSA I.D Casing I.D				Driller's o	or Firm's Name	onmental, In). Box 2379,	C	417 Certificate No c, ND 5850	
ÿ	TriconeO.D				Signed b	у			Date	8
	Method of development: Jet Surge	Air .BailX							BR/	IUN

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	PROJ	ECT: B	FAX-91-	020A	BORING: MW-30							
		C	ITY OF I	COLOGIC ASSESSMENT DICKINSON SANITARY LANDFILL N, NORTH DAKOTA	LOCAT 139-9	ION: 95-17	DBA					
					DATE:	9/2	1/92	SCALE: 1" = 10'				
(.190	Elev. 2453.4	Depth 0.0	ASTM Symbol	Description of Materials (ASTM D 2488)		BPF	WL	Tests or Notes				
ē				SPOILS consists mainly of clay, silt, and grained sand, with proportions, thickn	nd feine							
termino	-		1 1 1 1 1 1 1 1 1 1 1 1 1 1	depth variable.	css, anu							
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1	BFAX-91	-020A	<u></u>	BRAUN - 12/1/92		 _	L	MW-30 page 1 of 2				

PROJECT: B	FAX-91	-020A	BORING: MW-30 (cont.)							
С	ITY OF	EOLOGIC ASSESSMENT DICKINSON SANITARY LANDFILL ON, NORTH DAKOTA	LOCAT 139-		ON: 5-17DBA					
			DATE:	9/2	1/92	2	SCAL	E: 1	" = 10'	
Elev. Depth	ASTM Symbol			BPF	WL	Te	sts	or	Notes	
2335.4 1180 2335.4 1180 2322.9 130.5	SP	CLAY with silt, gray (5Y 5/1), occas organic blebs less than 1/2 inch diam damp. POORLY GRADED SAND medium greenish gray (5GY 5/1), little clay, waterbearing. END OF BORING END OF BORING	eter,			#8(1 Wate (113 #9(1) SCR FRC #10 #11	09-1 0 fee 14-1 EEN 0M 11 (119- (124- (129-	el at 2 et BG 15.5) 17.9 T 120.5) 125.5)	2340.40 S) ALLED O 127.9.	

Ci tu					vinces MD
		Proj. NoBFAX		Date of	kinson, ND
Well Number Date of					9/24/92
Revision		Crew_WS, PH	I, SB	_B.M. Location 8	. Elev. (± 0.01)
·	<u> </u>		*****		
Stick up above gi (to 0.1')	round 2.12	· [======]			
Top of riser pipe (w/o cap) Elev. (±0.01')	2374.72		GUARD POST: Type <u>T-Posts</u> Number <u>3</u>		Protective Cover: Type <u>None</u> Length <u>Lock # 2106</u>
Ground surface Elev. (±0.1')	2372.6		Type of sealin	g material <u>Vo</u>]	clay Bentonite Grout
Depth to bottom	2.5			RISER PIPE:	
of surface seal				Type Diameter	<u>PVC</u> 2"
				Total Length	27.52
Approximate wate level before			:	Sections Used	<u>3 plus 16" coup</u> ler
installation	28		Сар	Couplings Yes	<u>Flush-Thread</u>
Approximate dept of first water encountered in			Cap		
drilling	31		TYPE OF GROUT ABOVE SI	AL: Volclay	Bentonite Grout
			Amount of material used	50 gallon	
			Proportions 25 gallons	per 50 lb bag	grout
Depth to top of seal	23.02		TYPE OF SEALING MATER Amount of material used		
Depth to bottom of seal	25.02				
Denth de des			TYPE OF FILTER MATERIA		and $(12-30)$
Depth to top of screen	27.02		Amount of material used	4 bags (400 IDS)
			SCREEN		
			Type Slot Size	0.010	
			Lengtl	10'	
			Diamete		
Depth to bottom of screen	37.02		Plug/Poin	t <u>Plug</u>	
Depth to bottom of boring	2		DRILLER'S CERTIFICATIO This well was drilled under the best of my knowledge.	my jurisdiction,	and this report is true to
Method of advanc	. .		Braun Intertec Envir Driller's or Firm's Name	onmental, Inc	• <u>417</u> Certificate No.
HSA <u>X</u> Casing	I.D. <u>3 3/4"</u> I.D.		913 S. 18th St., P.C Address	<u>. Box 2379, B</u>	ismarck, ND _58502-2379
Tricone	_0.D		Signed by		Date
Method of develop	Air				BRAUN
Jet Surge	Bail <u>X</u>				

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	PROJ	ECT: B	FAX-91	-020A	BORING: TMW-1						
		C	ITY OF	EOLOGIC ASSESSMENT DICKINSON SANITARY LANDFILL ON, NORTH DAKOTA	KINSON SANITARY LANDFILL NORTH DAKOTA						
					DATE:	9/23	<u>3/92</u>	: so	CAL	E:	1" = 10'
(.290	Elev. 2372.6	Depth 0.0	ASTM Symbol	(ASTM D 2488)		BPF	WL	Test		or	Notes
lates for evaluation and descriptive	2372.6 2371.1 	0.0	Symbol		with ry fine ly, with an rained rained, oist.	BPF		PRP- TWT- TWT- INSTA FROM	2 (0 -3 (4 -4 (9- -4 (9-))))))))))))))))))))))))))))))))))))	to 1(-6) -11) ED S to 3 1 at 2	0 feet)
	-			X							
Ê	FAX-91-			BDATIN - 19/1709]]						

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City of Dist					kinon NI)
met 0	inson			Date of	kinson, ND 9/24/92
Data of		_Well Location			
Revision	<u></u>	_Crew_W3, FR,		_B.M. Location &	Elev. (±0.01)
Stick up above ground (to 0.1')					
Top of riser pipe (w/o cap) Elev. (±0.01')	2372.85		GUARD POST: Type <u>T-Post</u> Number <u>3</u>	S	Protective Cover: Type <u>Stæ1</u> Length <u>5'</u> Lock # <u>2106</u>
Ground surface Elev. (±0.1')2370	0.5		Type of sealin	g material <u>Volc</u>	lay Bentonite Grout
Depth to bottom of surface seal				RISER PIPE: Type · Diameter	PVC
Approximate water level before installation				Total Length Sections Used Couplings	26.96 3 plus 16" coupler Flush-Thread X No
Approximate depth of first water encountered in drilling			Cap TYPE OF GROUT ABOVE SI Amount of material used	EAL: Volclay I	
Depth to top of seal Depth to bottom of seal	<u>22.96</u> 24.96		Proportions <u>25 gallons</u> TYPE OF SEALING MATER Amount of material used	IAL: Bentonite	grout e Pellets 5 gallon bucket)
Depth to top of screen	_26.96		TYPE OF FILTER MATERIA Amount of material used	L: <u>Silica S</u> <u>4 bags (4</u>	and (12-30) 400 lbs)
			SCREEN Typ Slot Siz Lengt Diamete Plug/Poin	e <u>PVC</u> e <u>0.010</u> h <u>10'</u> rr <u>2''</u>	
Depth to bottom of screen			-		
Depth to bottom of boring	_38		DRILLER'S CERTIFICATIO This well was drilled under the best of my knowledge	my jurisdiction,	
			Braun Intertec Envir Driller's or Firm's Name	onmental, Inc.	417 Certificate No.
Method of advance: HSA X I.D. Casing I.D. I.D.	<u></u>			. Box 2379, Bi	smarck, ND 58502-2379
Tricone0.D	. <u>,</u>		Signed by		Date
	Air BailX				BRAUN

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LOG OF BORING

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PROJ	ECT: B	FAX-	·91-	020A	BORING: TMW-2									
	С	ITY (OF I	COLOGIC ASSESSMENT DICKINSON SANITARY LANDFILL N, NORTH DAKOTA	LOCATION: 139-95-17DBD									
					DATE:	9/2	3/92)2 SCALE: 1" = 10'						
Elev.	Depth 0.0	AST Sym		Description of Materials (ASTM D 2488)		BPF	WL	Tests or Notes						
Chevination and the set of the se		Sym			on o med very	BPF								

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APPENDIX E

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WATER-LEVEL TABLES

DICKINSON LANDFILL WATER LEVELS 8/03/93 TO 9/21/93

139-095-1 Sentinel	7CAD2 Butte Aquifer				ft)=2485.01 t.)=158-168
Date	Depth to Water (ft)	WL Elev (msl, ft)	Date	Depth to Water (ft)	WL Elev (msl, ft)
08/11/93 08/19/93 09/02/93	143.32 143.40 143.17	2341.69 2341.61 2341.84	09/08/93 09/21/93	143.32 143.31	2341.69 2341.70

139-095-17CAD1 (MW-27)

<u>Sentinel</u>	Butte Aquifer		SI (ft.)=126-136							
Date	Depth to Water (ft)	WL Elev (msl, ft)	Date	Depth to Water (ft)	WL Elev (msl, ft)					
08/11/93 08/19/93 09/02/93	132.39 133.46 133.49	2352.59 2351.52 2351.49	09/08/93 09/21/93	133.40 133.49	2351.58 2351.49					

LS Elev (msl,ft)=2484.98

139-095-1	7DAB		IS Elev (msl,ft)=2440.2						
Sentinel	Butte Acuifer		SI (ft.)=122-13						
Date	Depth to Water (ft)	WL Elev (msl, ft)	Date	Depth to Water (ft)	WL Elev (msl, ft)				
08/09/93	99.42	2340.80	09/08/93	100.19	2340.03				
09/03/93	99.76	2340.46	09/21/93	99.74	2340.48				

139-095-1	7 DBA (MW-30)		LS Elev (msl,ft)=24					
Sentinel	Butte Aquifer		SI (ft.)=122.9-1					
Date	Depth to Water (ft)	WL Elev (msl, ft)	Date	Depth to Water (ft)	WL Elev (msl, ft)			
08/10/93	112.82	2340.28	09/08/93	112.86	2340.24			
09/02/93	112.83	2340.27	09/21/93	112.75				

	7DCA (TMM-1) Butte Aquifer		LS Elev (msl,ft)=2372.6 SI (ft.)=27.02-37.02						
Date	Depth to Water (ft)	WL Elev (msl, ft)	Date	Depth to Water (ft)	WL Elev (msl, ft)				
09/03/93 09/08/93	27.92 27.88	2344.68 2344.72	09/21/93	27.85	2344.75				

139-095-1	7DCB		LS Elev (msl,ft)=2463.5						
Sentinel	Butte Aquifer		SI (ft.)=150-16						
Date	Depth to	WL Elev	Depth to WL E.						
	Water (ft)	(msl, ft)	Date Water (ft) (msl,						
08/10/93	113.59	2349.92	09/08/93	121.90	2341.61				
09/02/93	121.94	2341.57	09/21/93	121.86	2341.65				

139-095-17DAC (MH-29)

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LS Elev (msl,ft)=2446.46

<u>Sentinel</u>	Butte Aquifer		<u>SI (ft.)=125.5-135.5</u>							
Date	Depth to Water (ft)	WL Elev (msl, ft)	Date	Depth to Water (ft)	WL Elev (msl, ft)					
08/10/93 09/02/93	105.65 105.60	2340.81 2340.86	09/08/93 09/21/93	105.68 105.59	2340.78 2340.87					

APPENDIX F

MAJOR ION AND TRACE-ELEMENT CONCENTRATIONS

Dickinson Municipal Landfill Major Ion Analyses

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	Screened		I ((mill:	igram	s per	liter)							} Spec		
Location	Interval (ft)	Date Sampled	510 ₂	Fe	Mn	Ca	Mg	Na	ĸ	нсоз	со ₃	so	c1	F	NO3	в	TDS	Hardness CaCO ₃	NCH	Na	SAR	Cond (µmho)	Temp (∞C)	рН
139-095-17CAD2	158-168	09/02/93	16	0.31	0.1	9	3	340	6	778	36	150	16	2.5	4.3	0.45	967	3 5	. (95	2 5	1428	9	8.84
139-095-17CAD1	126-136	09/02/93	11	0.1	0.08	1 2	6	590	5.2	1290	0	160	11	2	4.3	0.55	1440	5 5	i () 95	35	2160	9	7.55
139-095-17DAB	122-132	09/03/93	37	0.5	0.11	13	5	410	10	782	5	330	16	2	8.9	0.37	1220	5 3	6 () 93	24	1713	. 7	8.27
139-095-17DBA	122.9- 127.9	09/02/93	34	0.72	0.03	6	1	390	7.2	804	200	110	14	2.9	15	0.53	1180	19	•	97	39	1625	i S	9 9.97
139-095-17DCA	27.02- 37.02	09/03/93	69	1.3	0.22	9	4	450	4.5	1270	0	76	18	1.6	10	0.67	1270	3 9		96	31	1792	<u>،</u> ۱	9 7.47
139-095-17DCB	150-160	09/02/93	11	0.16	0.21	33	15	810	11	1690	0	600	20	1.2	8	1	2340	140)	92	30	3370) 10	0 7.34
139-095-17DAC	125.5- 135.5	09/02/93	10	0.3	0.07	9	4	490	6.1	1260	2 0	110	13	2.6	3.8	0.58	1290	3 9	•	9 9 6	34	1926		8 8.33

Trace Element Analyses

Location	Date Sampled	Selenium	Lead	Cadmium (micrograms p	Mercury er liter)~	Arsenic	Molybdenum	Strontium
139-095-17CAD2	9/2/93	0	2	0	0	15	15	190
139-095-17CAD1	9/2/93	0	0	D	0	1	12	450
139-095-17DAB	9/2/93	0	1	o	0	9	9	470
139-095-17DBA	9/2/93	o	2	0	0	3	9	200
139-095-17DCA	9/2/93	o	1	0	0	1	11	440
139-095-17DCB	9/2/93	o	0	0	0	3	3	1100
139-095-17DAC	9/2/93	0	1	0	0	1	3	330

APPENDIX G

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VOLATILE ORGANIC COMPOUNDS FOR WELL 139-095-17DAB

Volatile Organic Compounds and Minimum Concentrations

Concentrations are based only on detection limits. Anything over the detection limit indicates possible contamination.

Constituent	Chemical Analysis µg/L
Benzene	<2
Vinyl Chloride	<1
Carbon Tetrachloride	<2
1,2-Dichlorethane	<2
Trichloroethylene	<2
1,1-Dichloroethylene	<2
1,1,1-Trichloroethane	<2
para-Dichlorobenzene	<2
Acetone	<50
2-Butanone (MEK)	228*
2-Hexanone	<50
4-Methyl-2-pentanone	<50
Chloroform	<5
Bromodichloromethane	<5
Chlorodibromomethane	<5
Bromoform	<5
trans1,2-Dichloroethylene	<2
Chlorobenzene	<2
m-Dichlorobenzene	<5
Dichloromethane	<5
cis-1,2-Dichloroethylene	<2
o-Dichlorobenzene	<2
Dibromomethane	<5
1,1-Dichloropropene	<5
Tetrachlorethylene	<2
Toluene	<2
Xylene(s)	<2
1,1-Dichloroethane	<5
1,2-Dichloropropane	<2
1,1,2,2-Tetrachloroethane	<5
Ethyl Benzene	<2
1,3-Dichloropropane	<5
Styrene	<2
Chloromethane	<5
Bromomethane	<5
1,2,3-Trichloropropane	<5
1,1,1,2-Tetrachloroethane	<5
Chloroethane	<5
1,1,2-Trichloroethane	<5

* Constituent Detection

VOC Constituents cont.

2,2-Dichloropropane	<5
o-Chloroluene	<5
p-Chlorotoluene	<5
Bromobenzene	<5
1,3-Dichloropropene	<5
1,2,4-Trimethylbenzene	<5
1,2,4-Trichlorobenzene	<5
1,2,3-Trichlorobenzene	<5
n-Propylbenzene	<5
n-Butylbenzene	<5
Naphthalene	<5
Hexachlorobutadiene	<5
1,3,5-Trimethylbenzene	<5
p-Isopropyltoluene	<5
Isopropylbenzene	<5
Tert-butylbenzene	<5
Sec-butylbenzene	<5
Fluorotrichloromethane	<5
Dichlorodifluoromethane	<5
Bromochloromethane	<5
Allylchloride	<5
2,3-Dichloro-1-propane	<5
Tetrahydrofuran	140*
Pentachloroethane	<5
Trichlorotrofluoroethane	<5
Carbondisufide	<5
Ether	<5

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* Constituent Detection